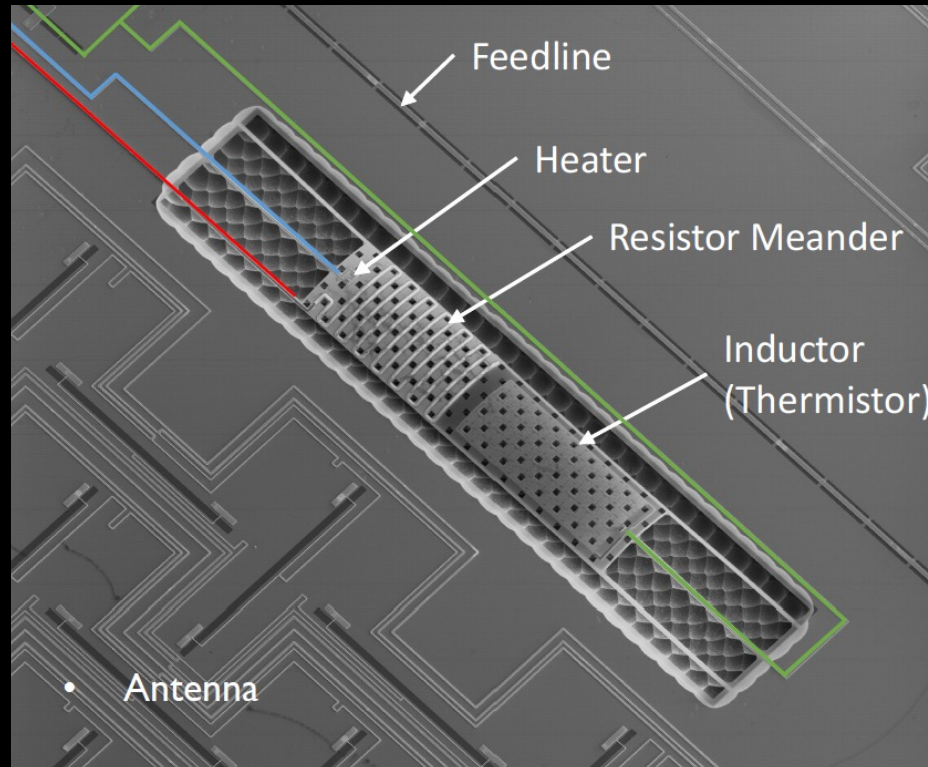


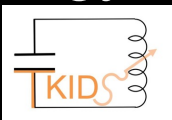
TKIDs for CMB and millimeter wave astrophysics



Roger O'Brient

Jet Propulsion Laboratory, California Institute of Technology

CPAD 2023- SLAC



Team Members



Albert Wandui

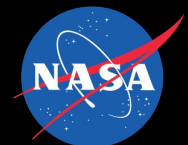


Lorenzo Minutolo

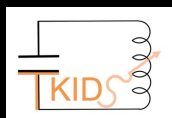


Bryan Steinbach

- Cliff Frez- JPL
- Anthony Turner- JPL
- Sophia Fatigoni Caltech
- Kenny Lau- Caltech
- Jamie Bock- Caltech
- Jonas Zmuidzinas- Caltech
- Zoe Smith- Stanford
- Taj Dyson- Stanford
- Shawn Henderson- SLAC
- Shub Agriwal- UPenn
- Katie Hughes- UChicago

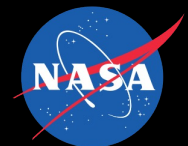


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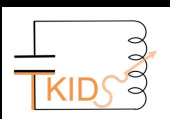


Outline

- Motivations
- Designs
- Performance
- What's next?

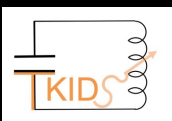
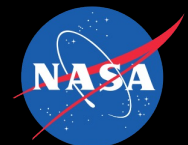


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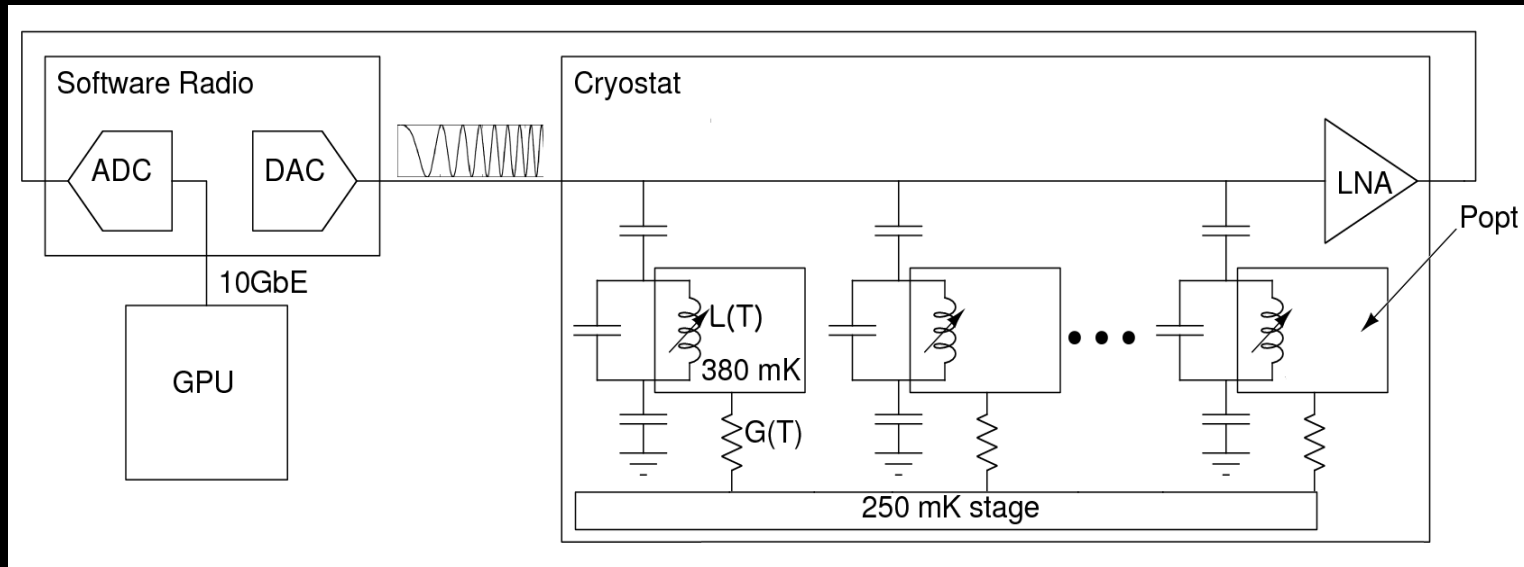


Scientific Applications

- Millimeter waves are crucial for cosmology
- Cosmic Microwave Background: post-S4 larger field maps
- Intensity line mapping:
 - CII to trace reionization
 - CO to trace cosmic expansion history through dark energy dominance
- All require large arrays of detectors



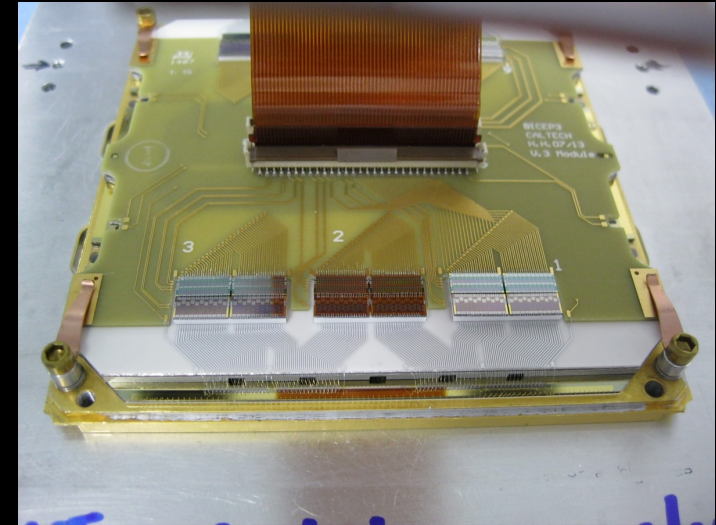
Thermal Kinetic Inductance Detectors



- Bolometer with kinetic inductance thermometer
- Inductors are in high-Q resonators, each with unique resonant frequency
- All inductors are in parallel from a common transmission line
- Fundamental detector noise is phonons in the legs, *not* GR

The merits of TKIDs

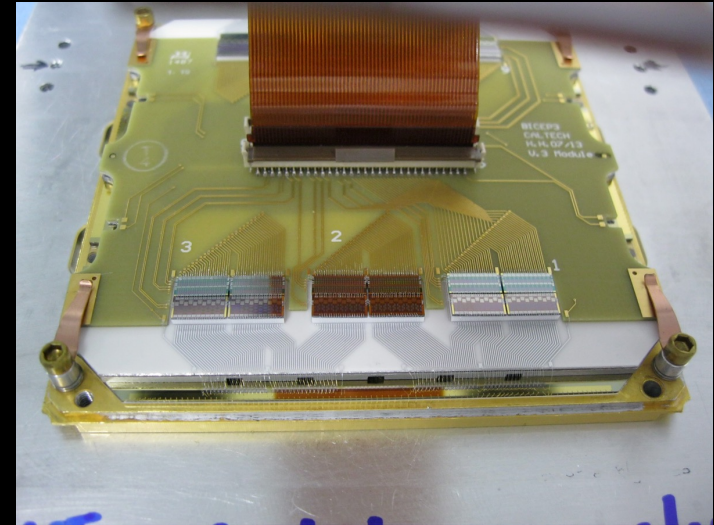
- No SQUIDs- simplified readout



Note all the ~1mm 3-D wirebonds (Nightmare fuel!)

The merits of TKIDs

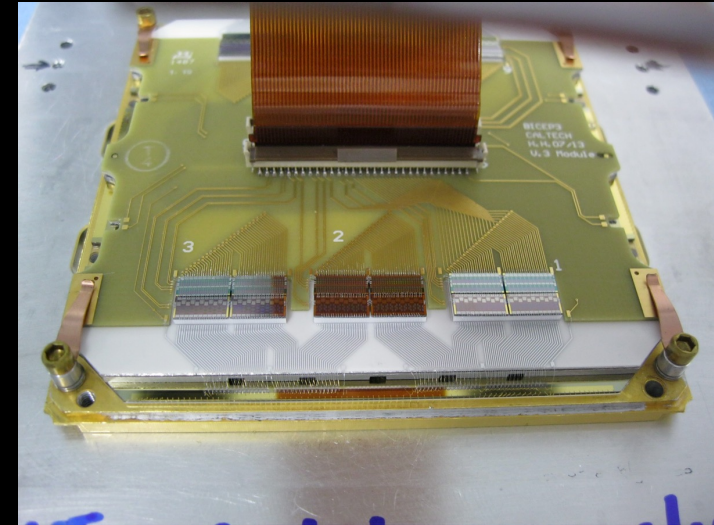
- No SQUIDs- simplified readout
- Retain many valuable bolometer features:
 - Ease of optical coupling
 - Natural radiation hardening
 - Can be background noise limited
 - Calibration of responsivity



Note all the ~1mm 3-D wirebonds (Nightmare fuel!)

The merits of TKIDs

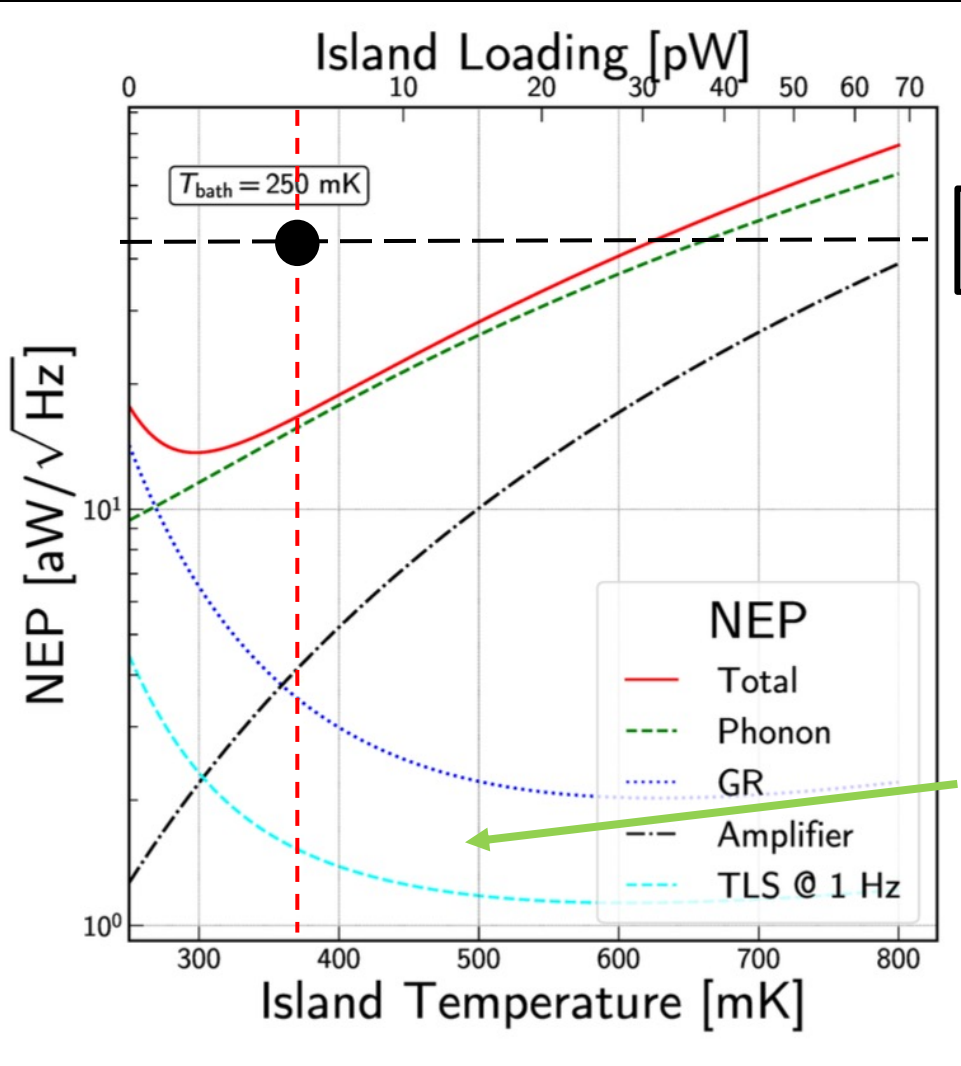
- No SQUIDs- simplified readout
- Retain many valuable bolometer features:
 - Ease of optical coupling
 - Natural radiation hardening
 - Can be background noise limited
 - Calibration of responsivity
 - Myriad design parameters:
 - T_c
 - T_{bath}
 - Inductor volume
 - T_{island}
 - Bolometer G
 - Inductor optical absorption efficiency



Note all the ~1mm 3-D wirebonds (Nightmare fuel!)

Sensitivity

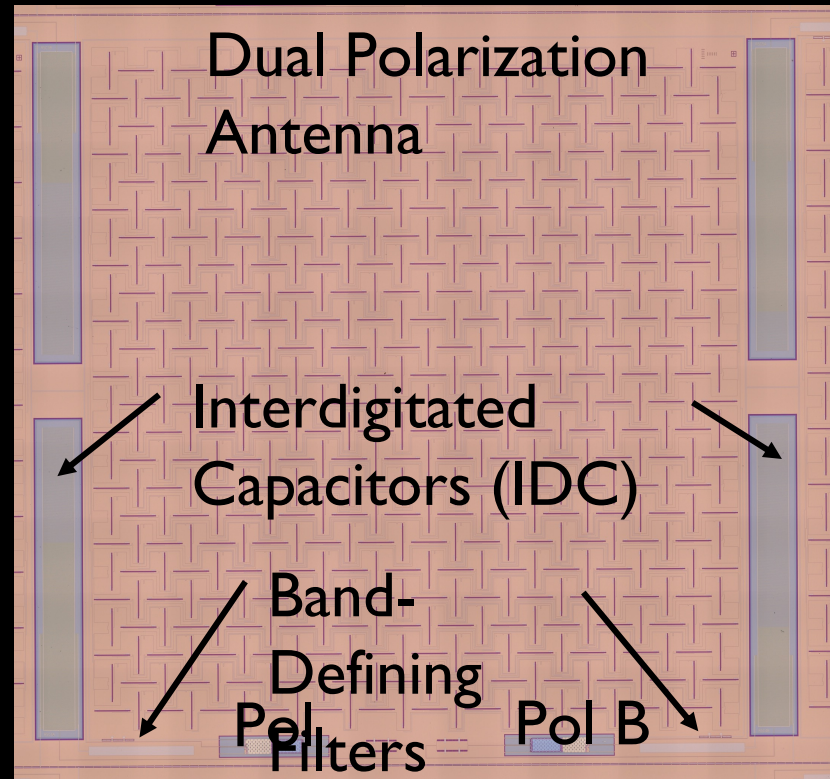
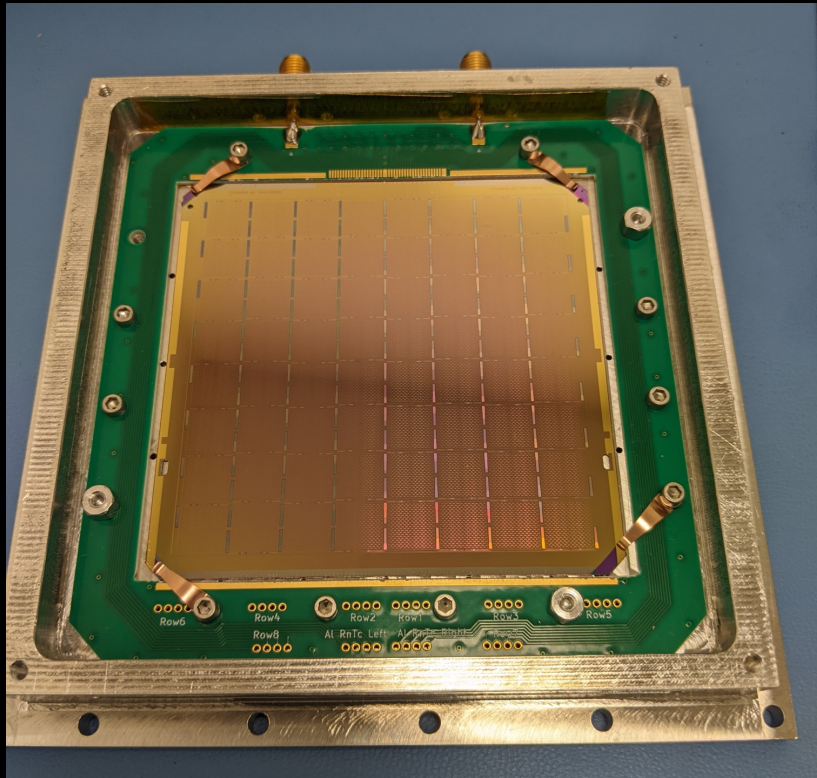
$$S = \frac{\partial f_r}{\partial P} = f_r(T) \frac{\beta(\omega, T) \kappa(T)}{2Q_i G(T) T}$$



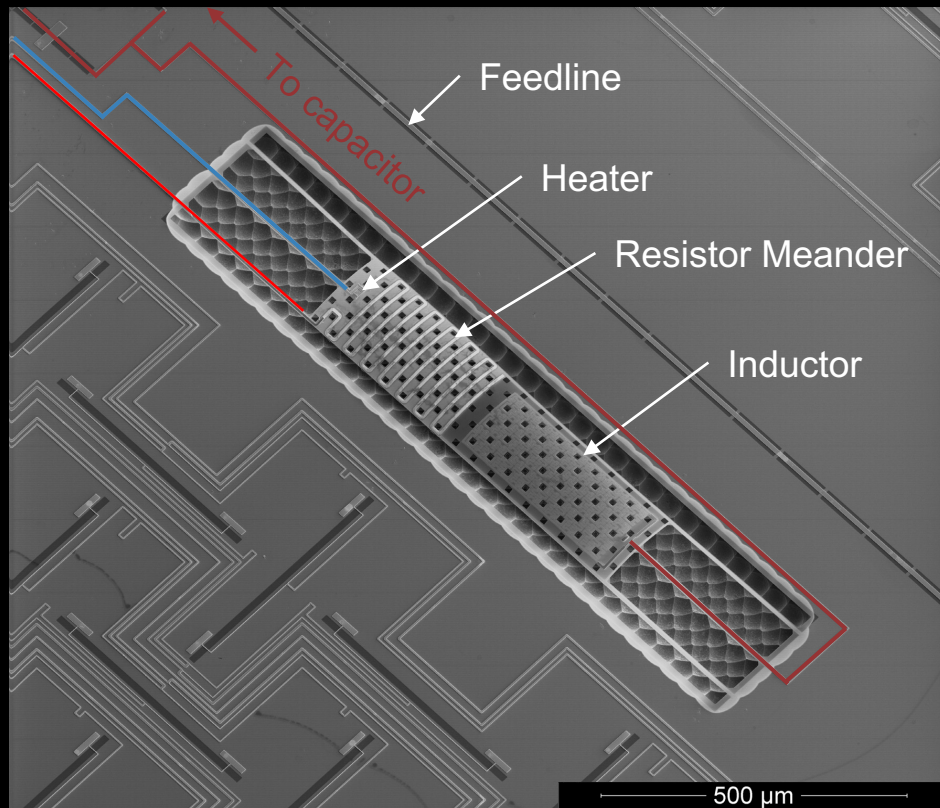
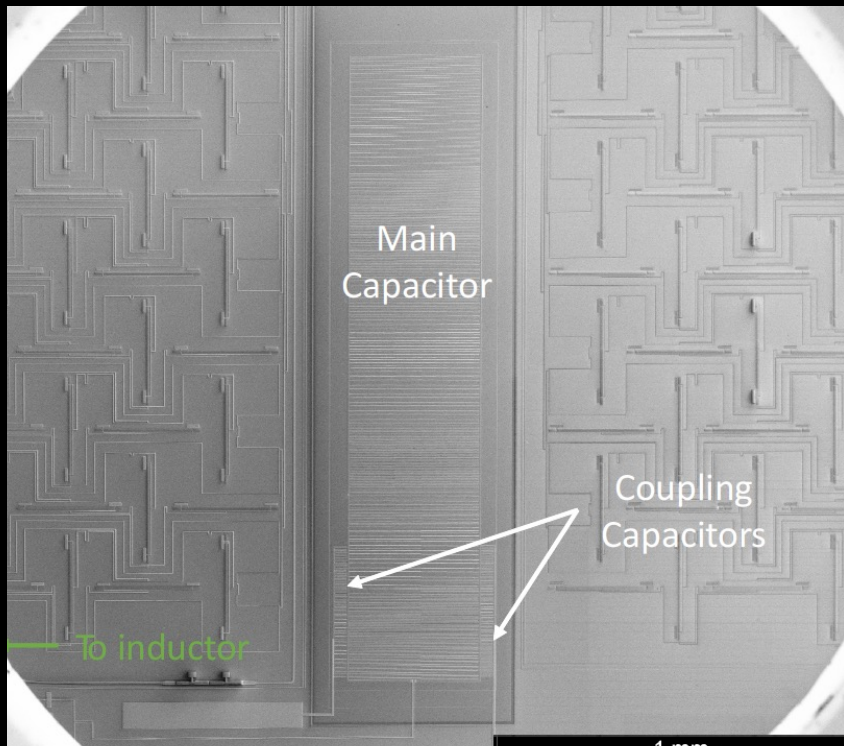
Expected Photon Noise

High responsivity suppresses GR and TLS noise at higher loading

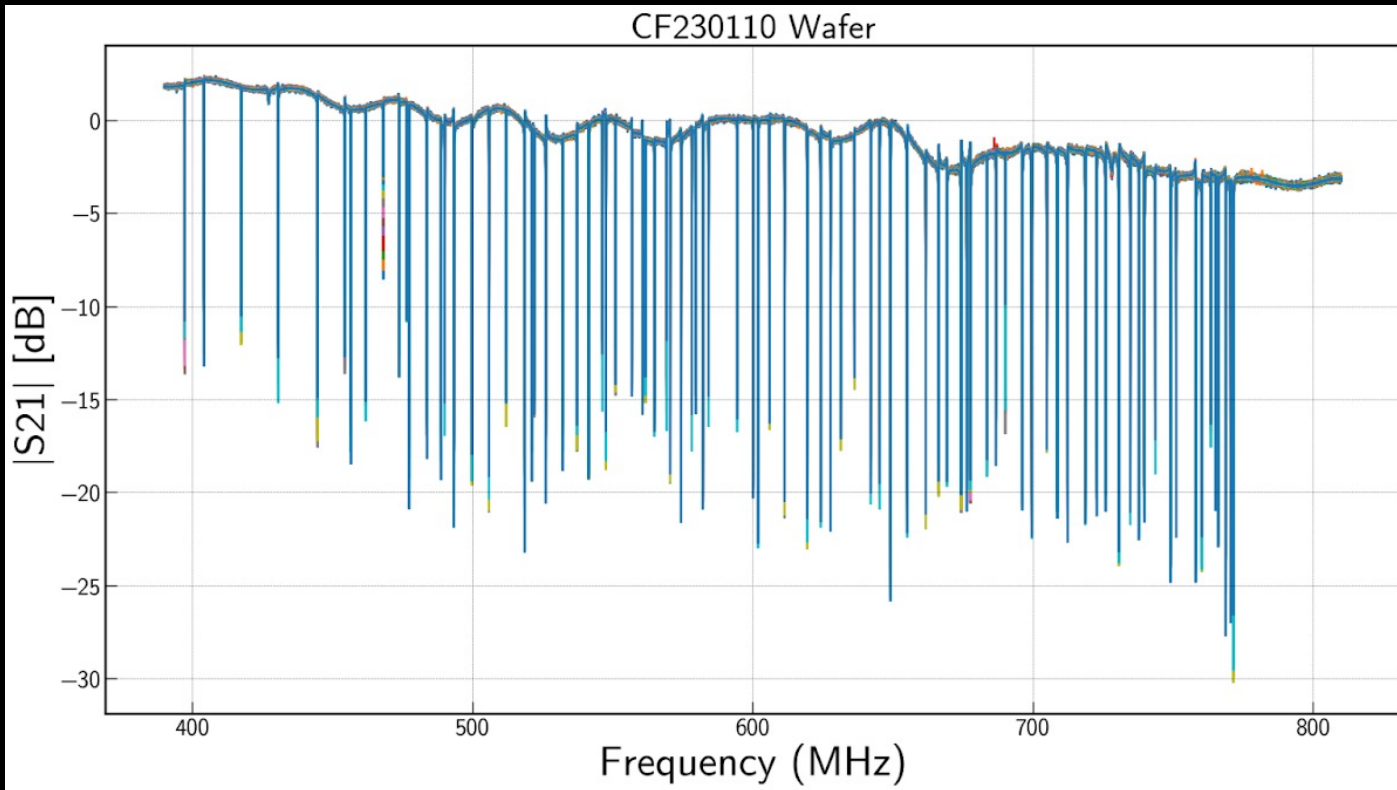
Detector Design



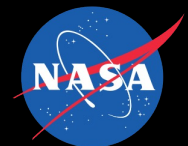
Detector Design



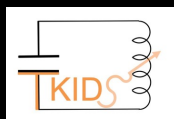
High yield arrays



- We use LED arrays to identify detectors with their resonance
- Capacitor trimming to avoid collisions
- Then release bolometers

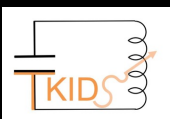
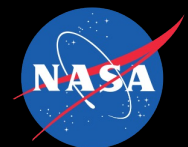
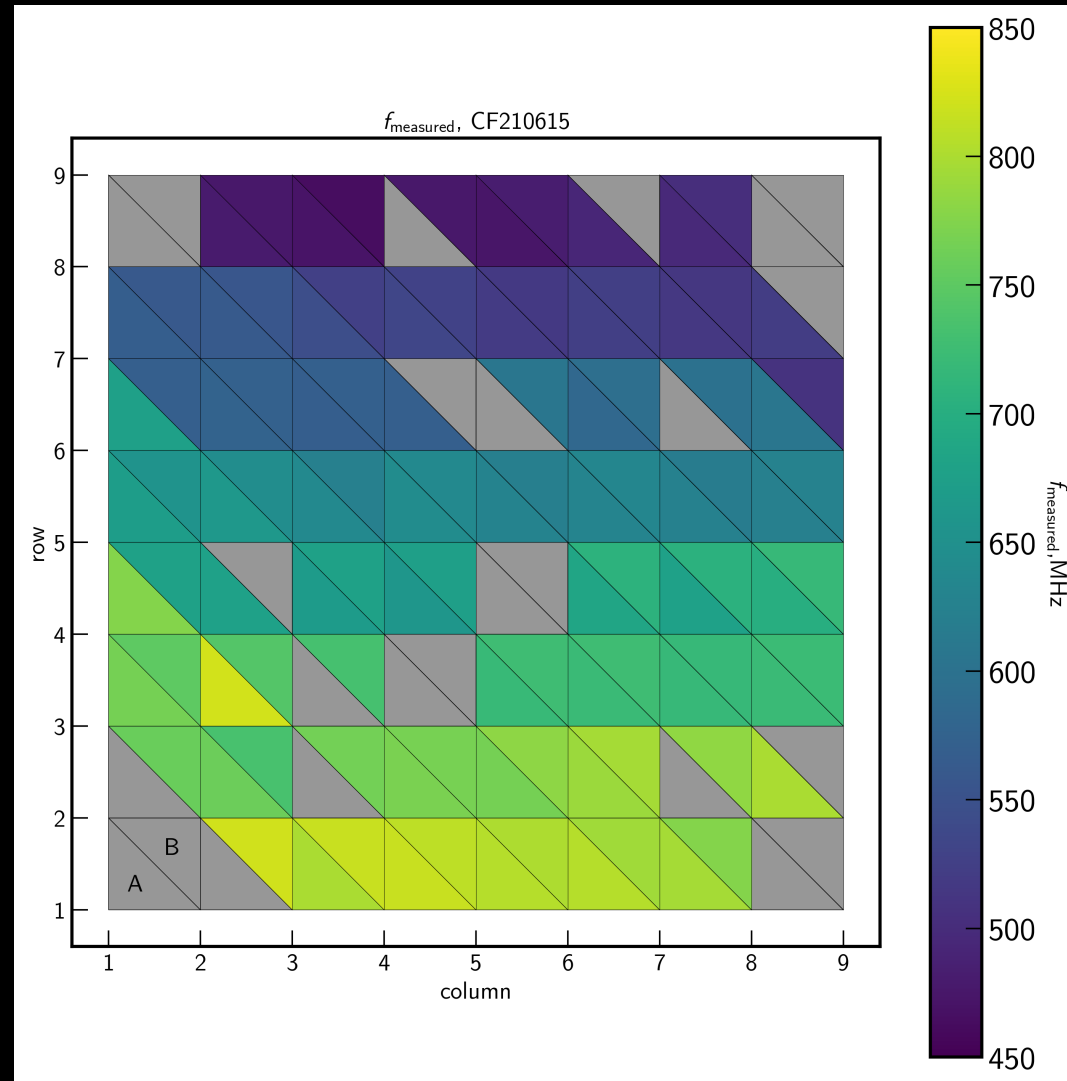


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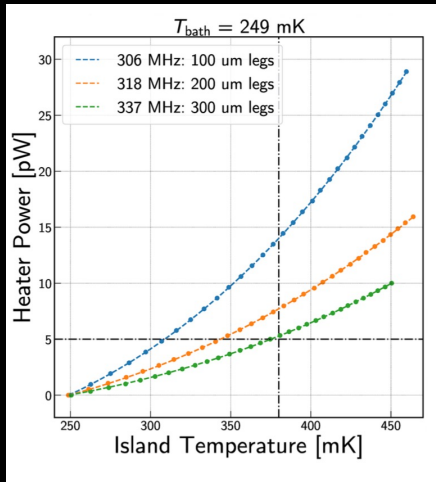


Yield

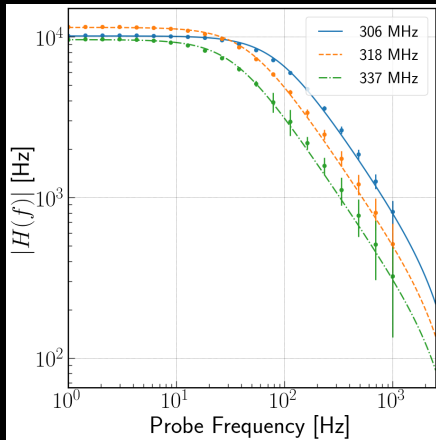
- Best yield on TKID tile: 112/128 detector pairs
- Have estimated defect density on capacitors through optical inspection: $0.299/\text{mm}^2 \pm 0.063$
- Feedline defects can be fatal.



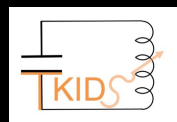
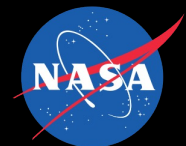
Bolometer & Inductor Properties



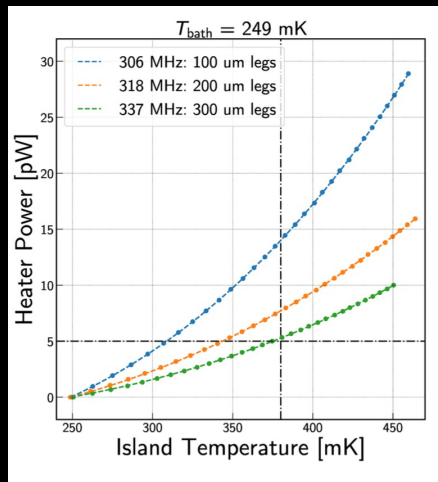
- Use calibration heater to vary island temperature
- Leg Thermal Conductivity G consistent with TES experience
- Temperature index $n \sim 3$.



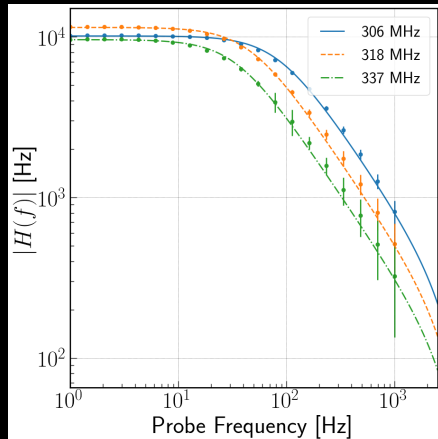
- Roll-off of transfer function from AC drive on heater
- Time constant set by island heat capacity as well as G
- Independent of island temperature
- No electrothermal feedback



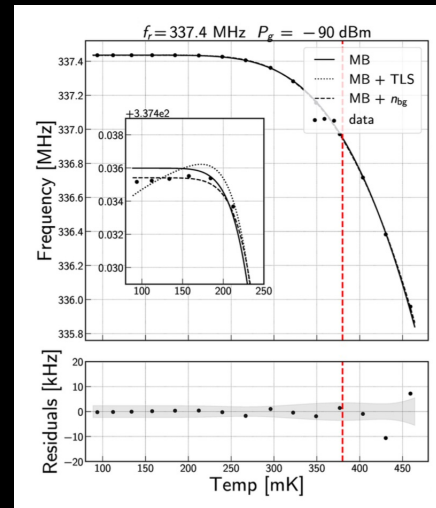
Bolometer & Inductor Properties



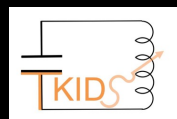
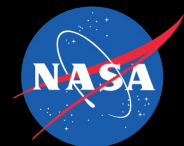
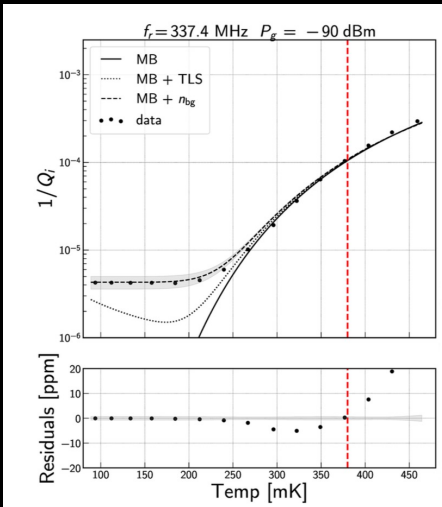
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- Roll-off of transfer function from AC drive on heater
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- Independent of island temperature
- No electrothermal feedback!

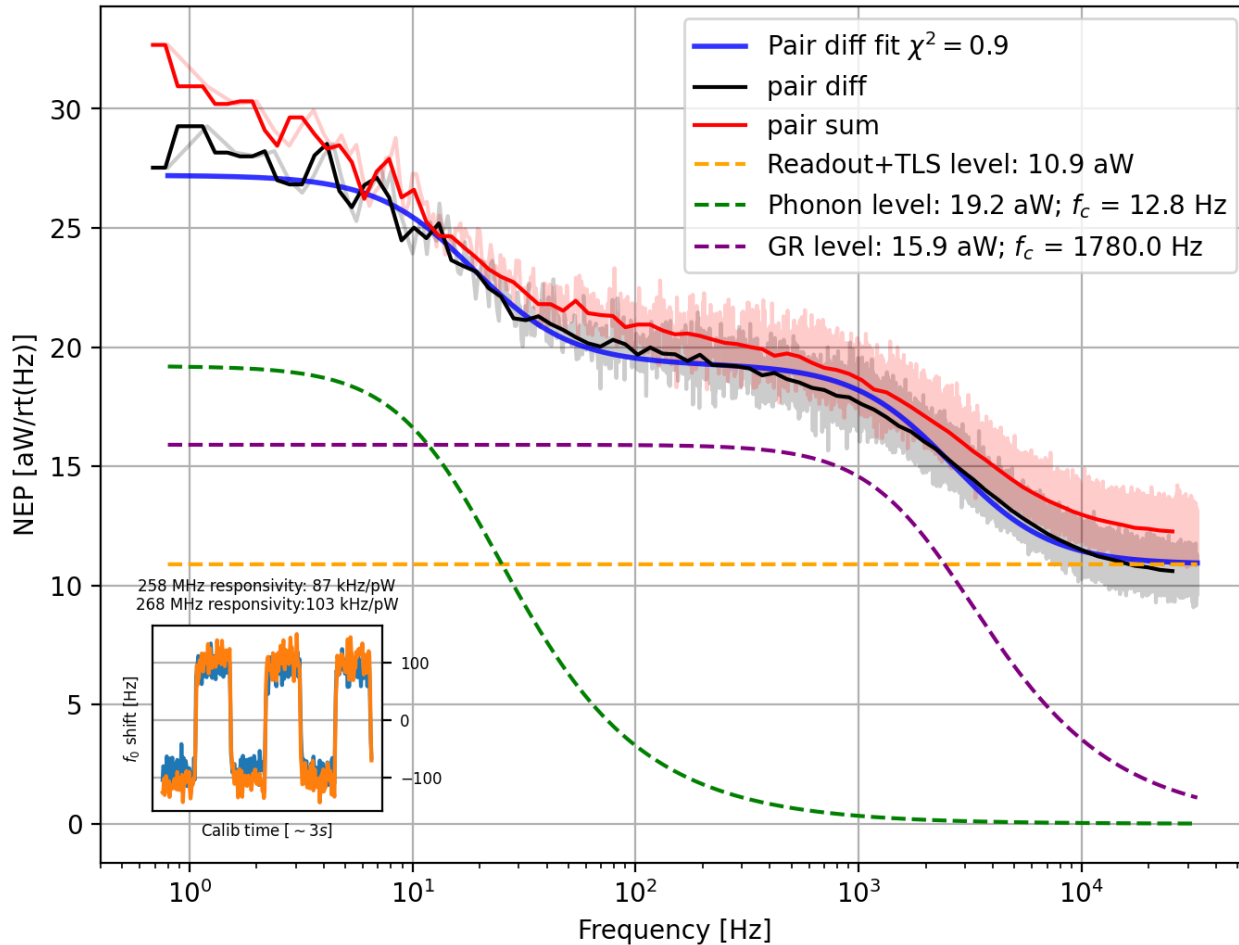


- Resonator Q and f_r vary with temperature
- Well described by Mattis Bardeen Theory on Aluminum
- There is a background quasiparticle background that limits Q_i
- Red line is intended operating temperature. Thermal quasiparticles dominate there

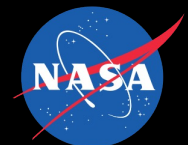


Noise Studies

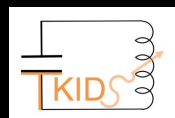
5.97pW optical bias, -96.1 dBm readout power



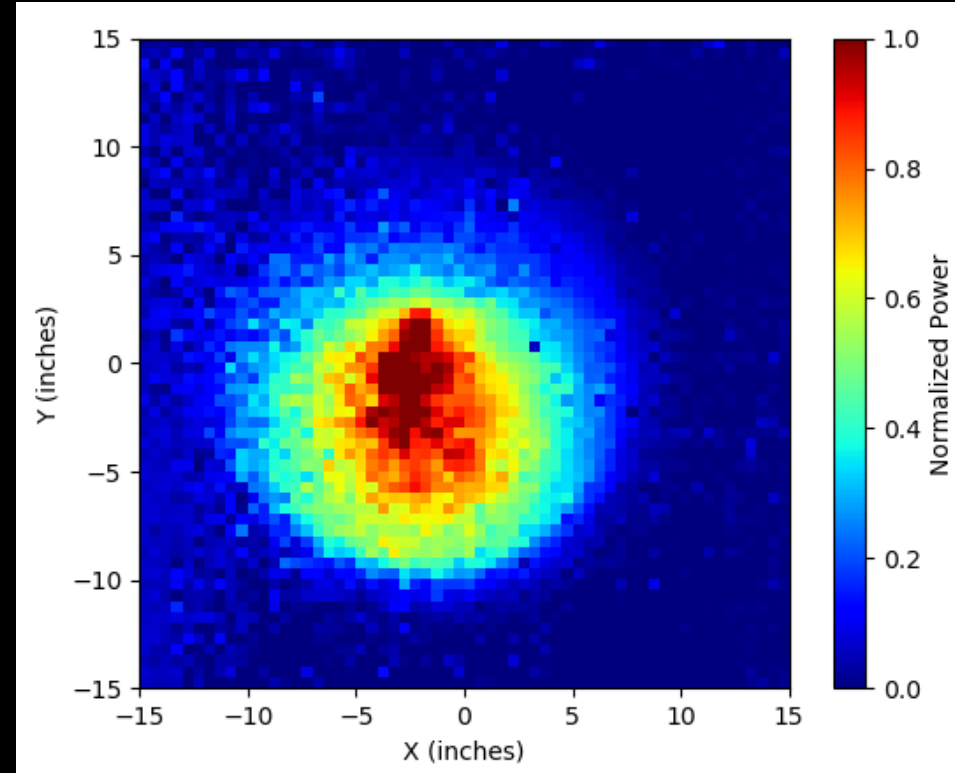
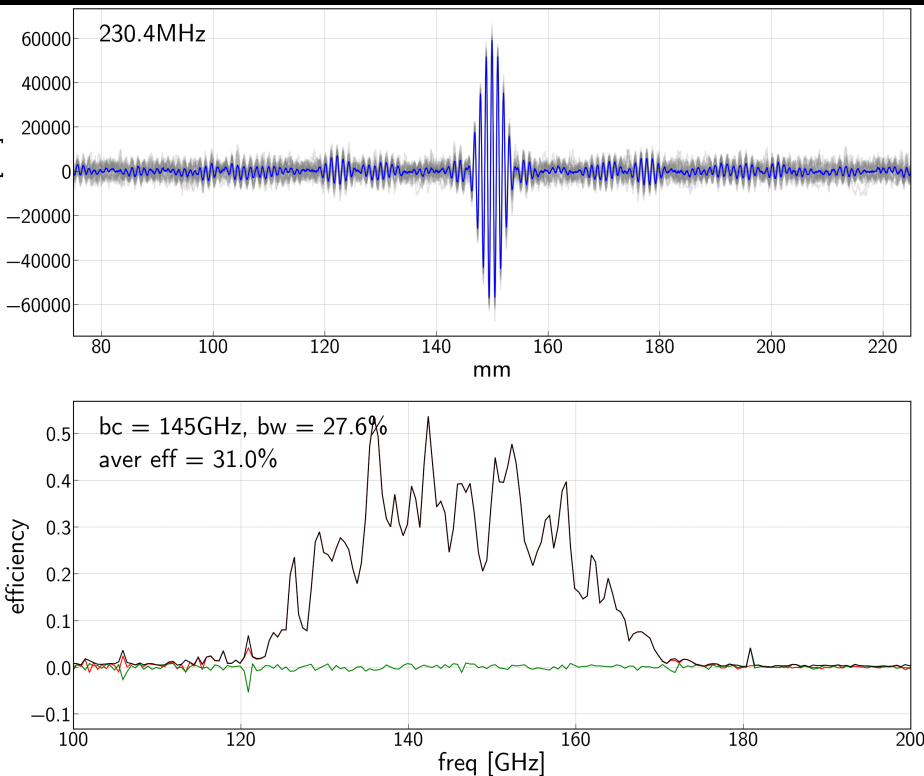
- We expect 6pW power for 150GHz at the South Pole.
- So bias heaters to provide that in lab
- Total noise is below the expected photon NEP~45aW/rtHz
- Pair difference is stable to low frequencies
- Dashed lines show model, with higher than expected GR noise, and longer lifetimes.



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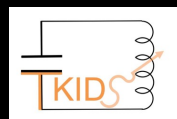
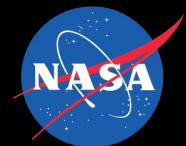


Optical Responsivity



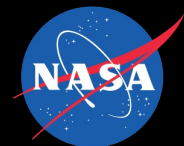
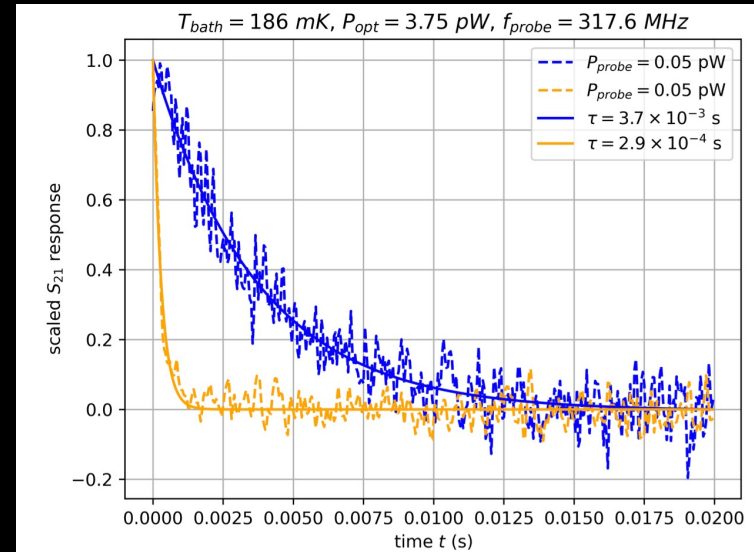
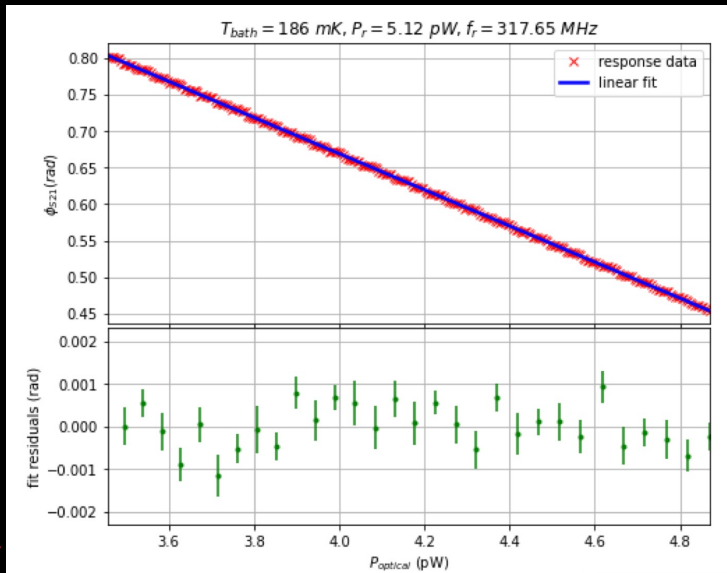
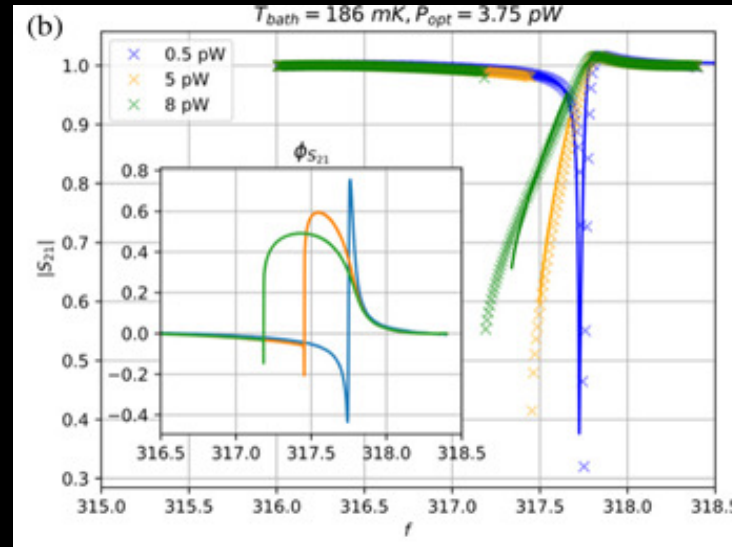
- Bands are as consistent with design, limited out of band response
- Camera Optical efficiency of ~30% (includes optical filters and window)
- Beams are roughly gaussian.
- Distortion at peak is due to internal reflections in the optics.
- Lines shift several line widths
- So we use a chirped readout

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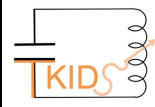


Electrothermal Feedback

arXiv: 2107.12493

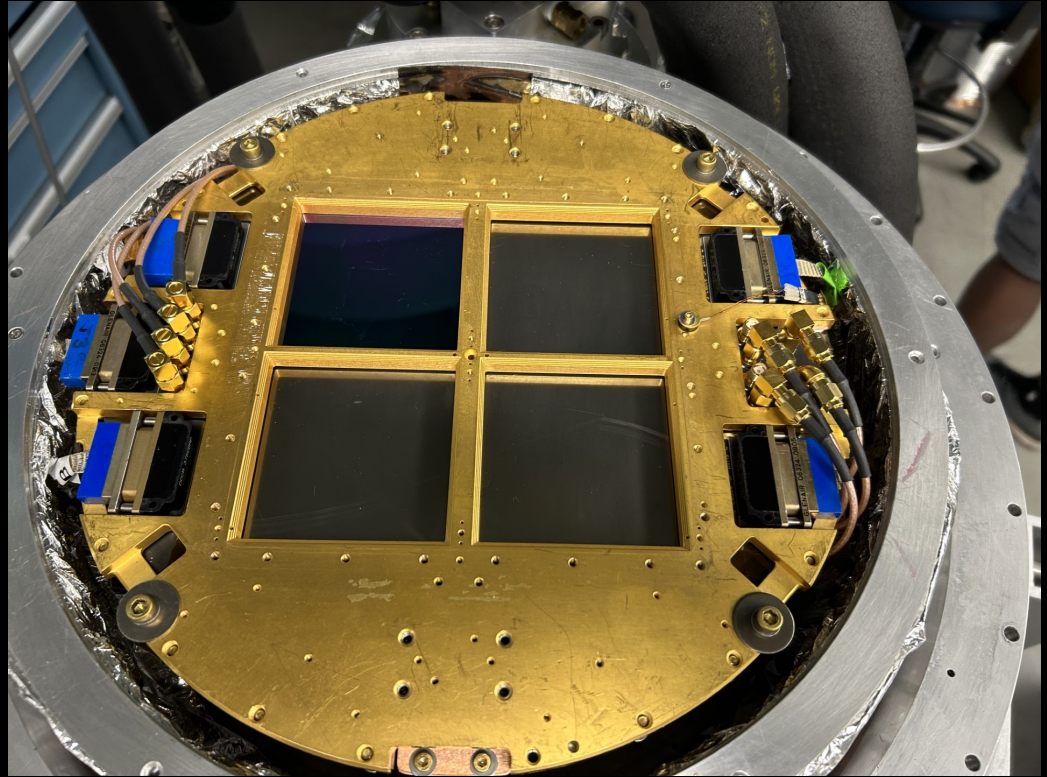


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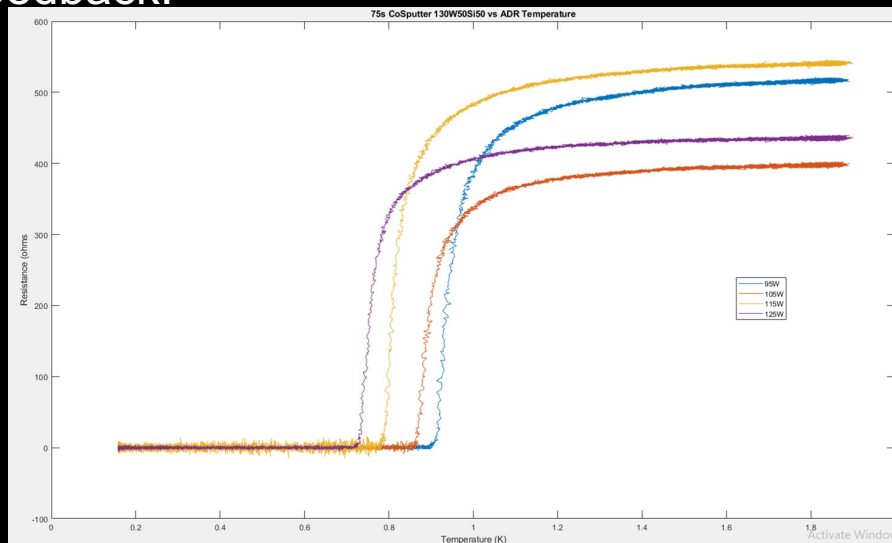
Field Demonstration

- Possible BICEP field demonstration
- We have four tiles of high yield arrays, and still testing others
- Retrofitted Keck Array Camera
- Have been conducting system level studies of the camera in the lab
- NSF has some infrastructure challenges to work through



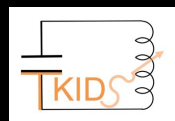
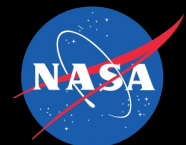
Lower loading TKIDs

- A CMB space observatory loading lower an order of magnitude lower than through atmosphere: 0.5-2pW
- Ground based spectrometers with $R \sim 100$ have similarly reduced loading compared to CMB photometric experiments
- We know we can build bolometers with leg G to be background noise limited
- Need to contain GR noise:
 - WSi T_c can be adjusted by varying film content with co-sputtering
- Lower G requires lower C to maintain similar time constants
- High resistivity inductor films are key to limiting island size. ($\rho_{\text{WSi}} \sim 100 \Omega/\square$)
- Electrothermal Feedback.

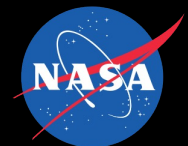


Courtesy of Andrew Beyer/
Sahil Patel

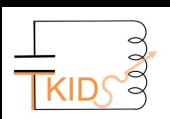
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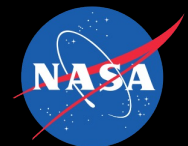
Thanks for your attention



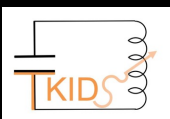
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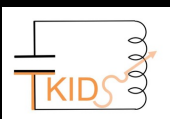
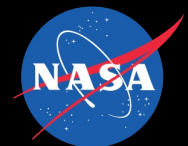
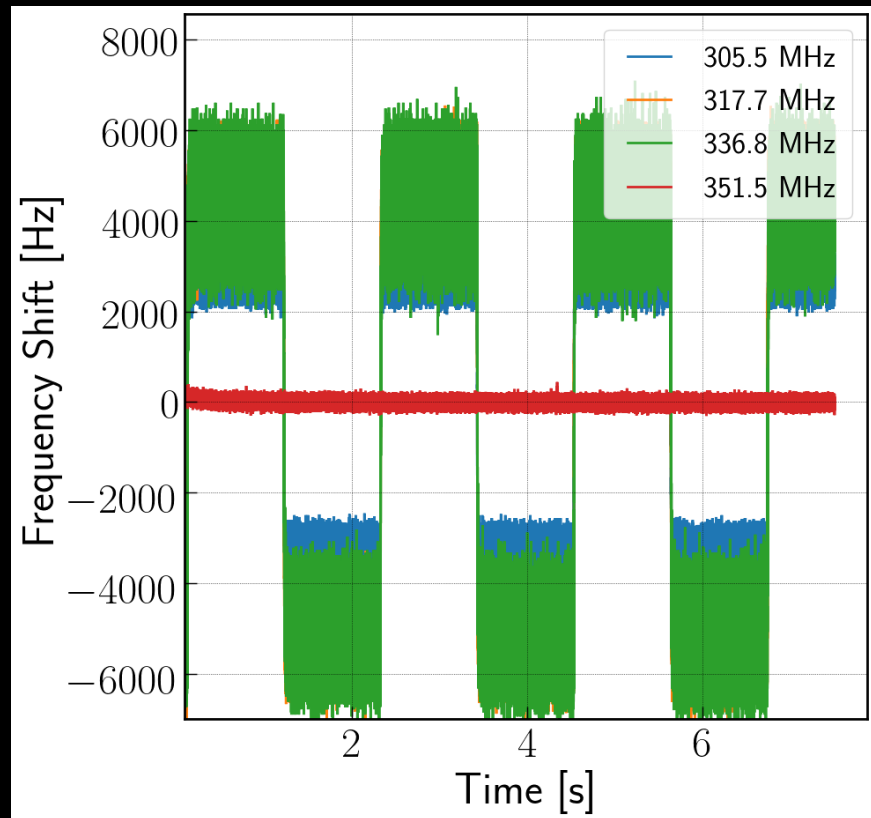
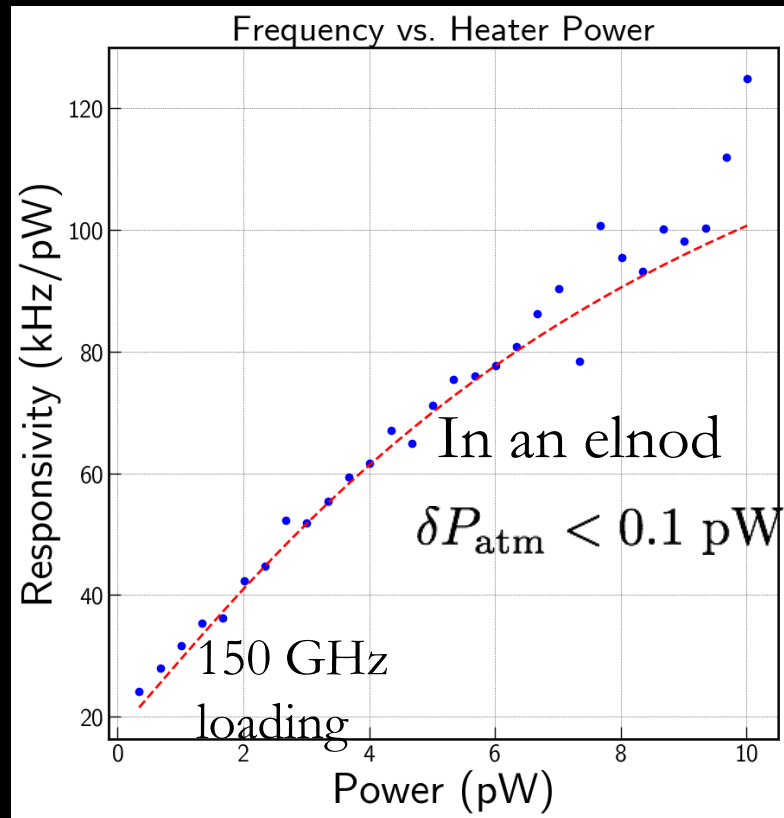
Extra slides



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Responsivity



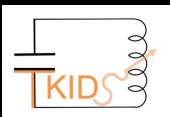
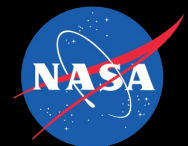
GR Noise

$$\text{NEP}_{gr}^2 = \frac{1}{V_{sc}^2 \cdot (\partial n_{qp} / \partial P_{opt})^2} S_{gr}$$

$$\text{NEP}_{gr}^2 = 4G(T_0)k_B T_0^2 \cdot \left(\frac{G(T_0)}{k_B \cdot \kappa(T_0)^2 n_{qp}(T_0)^2} \cdot \frac{1}{R^* V_{sc}} \right)$$

$$\text{NEP}_{ph}^2 = 4G(T_0)k_B T_0^2 \cdot F(T_0, T_{bath})$$

- QP density has an exponential dependence on temperature.
- At high enough temperature system reduces to a single-link system
- Qi drops at higher temperatures. Multiplexing sets a lower bound on Qi at operating temperature



TLS and Amp Noise

$$\text{NEP}_{\text{TLS}}^2 = \frac{1}{(\partial x / \partial P)^2} S_{\text{TLS}} \quad \text{NEP}_{\text{amp}} = \frac{1}{\partial x / \partial P_{\text{opt}}} \cdot \frac{2}{Q_i \chi_c \chi_g} \cdot \sqrt{\frac{k_B T_N}{P_g}}$$

$$S_{\text{TLS}} [\text{Hz}^{-1}] = \kappa_{\text{TLS},0} \left(\frac{\nu}{1\text{Hz}} \right)^{-1/2} \left(\frac{T}{380\text{mK}} \right)^{-2} (1 + N/N_c)^{-1/2}$$

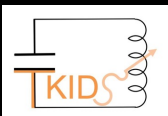
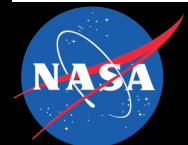
$$N = \frac{E_{\text{stored}}}{hf_r}$$

Microwave photon number given by energy stored and resonance frequency

$$S_{\text{TLS}} \ll 2.7 \times 10^{-17} \text{ Hz}^{-1}$$

At T=380 mK, responsivity is 33 l ppm/pW

- Cryogenic amplifier at 4K. Measured noise temperature of ~5K.
- Relation above is true even when the resonator is asymmetric.

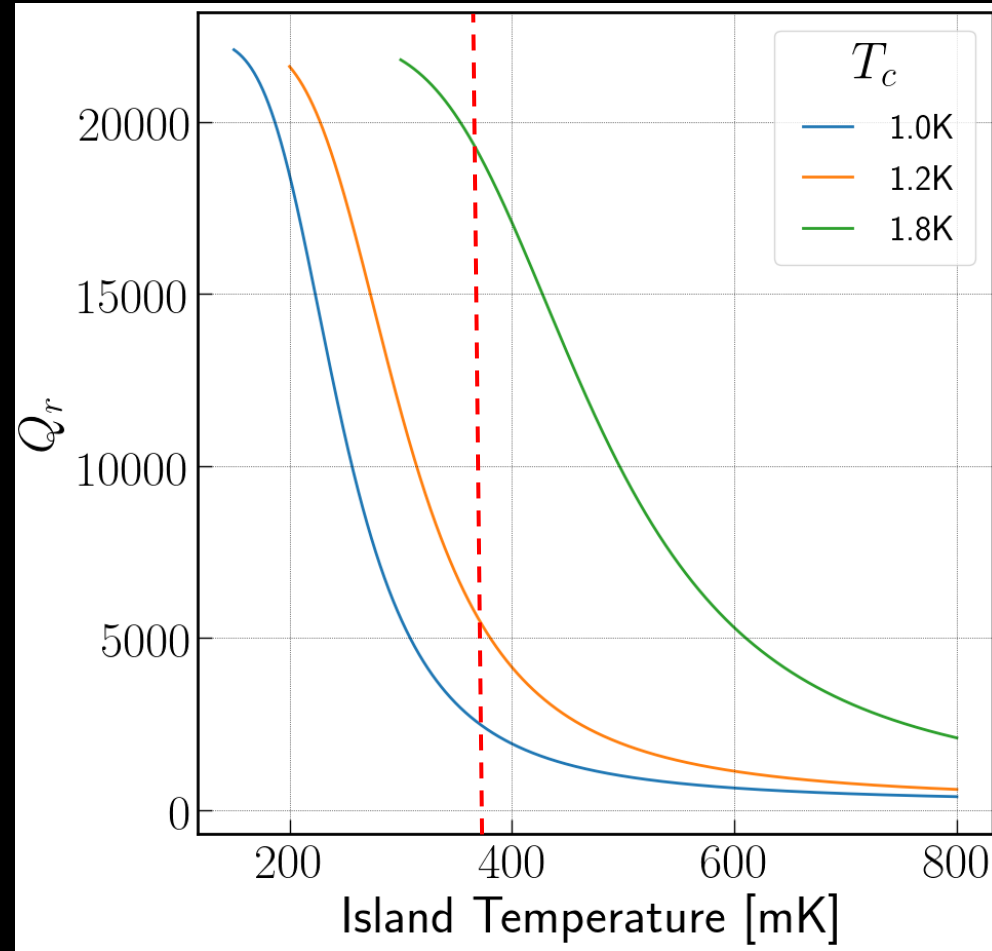


Readout Requirements

- Dynamic Range Requirement: -95dBc/Hz
- Bandwidth requirements: 256 devices across an octave of BW.
- To multiplex N=256 channels over m=1 octaves with $\xi=0.5\%$ cross talk, we require:

$$Q_r \approx N \xi_{max}^{-1/2} 2^m$$

- Requirements for warm lab testing set how tightly we can pack the resonators

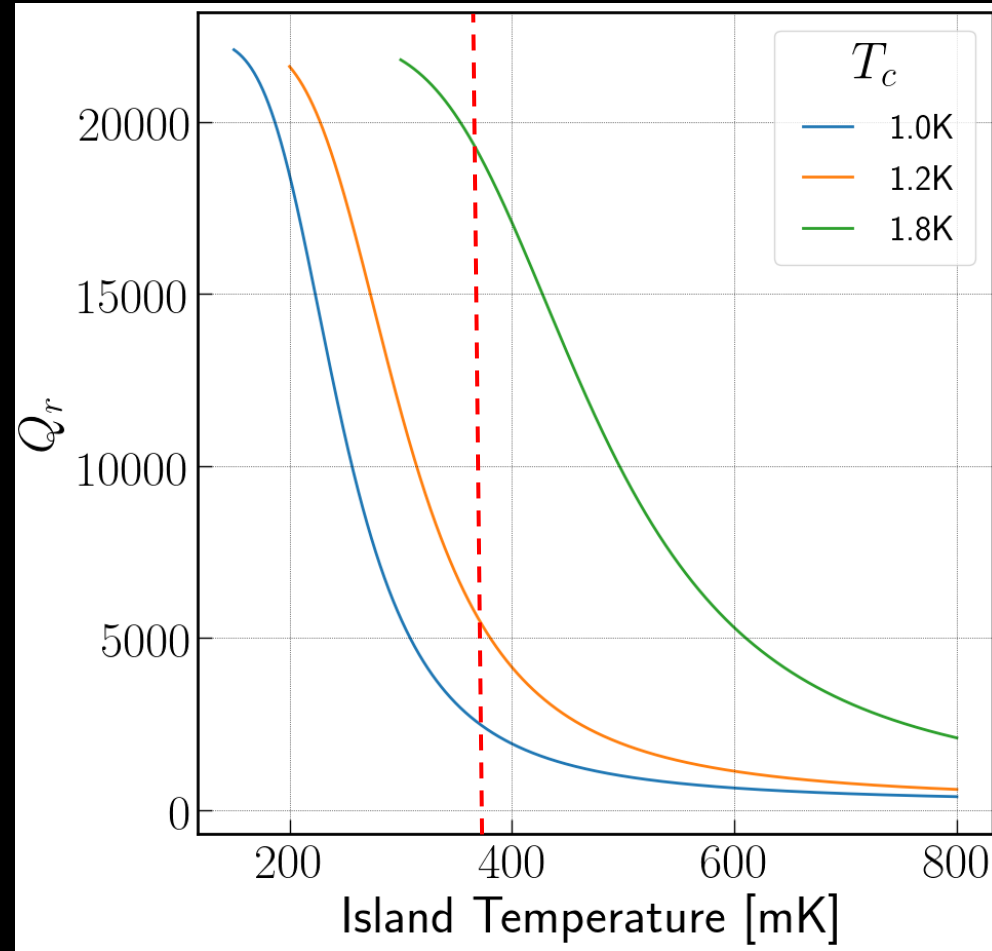


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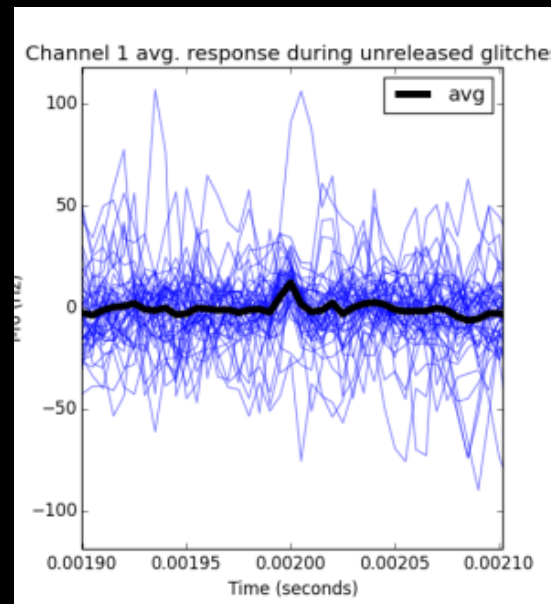
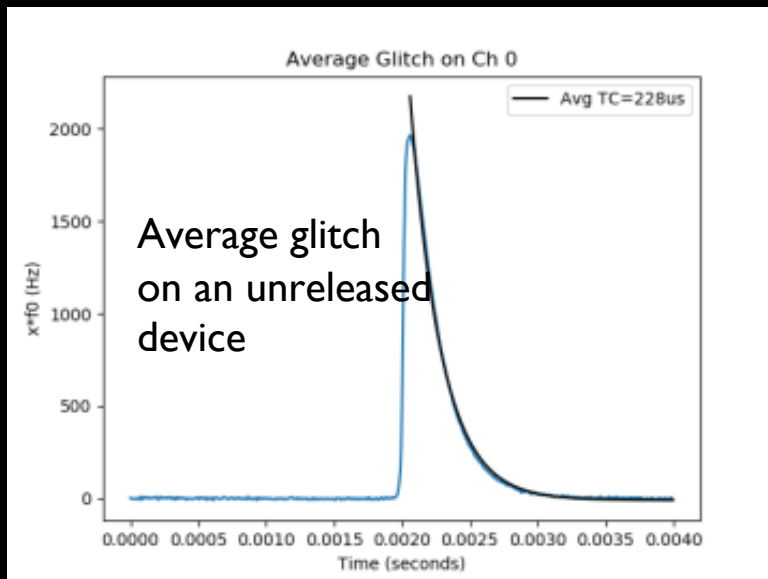
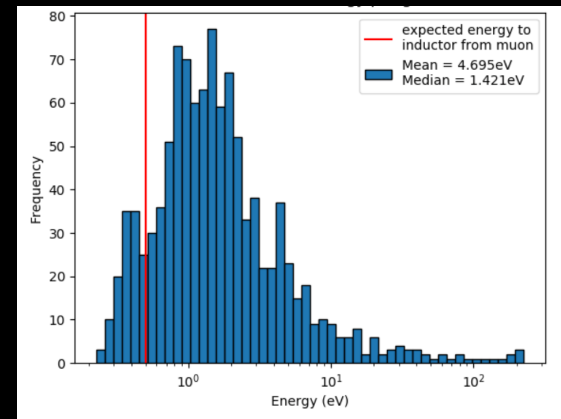
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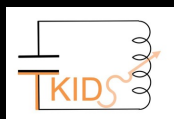
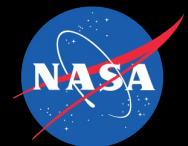
Cosmic Ray Testing

- Expected muon hit rate: 1 per second
- Can compare the glitch rate on the released vs. unreleased devices
- Checked for coincident cosmic ray hits using a scintillator
- Cosmic ray hits to measure qp time constants



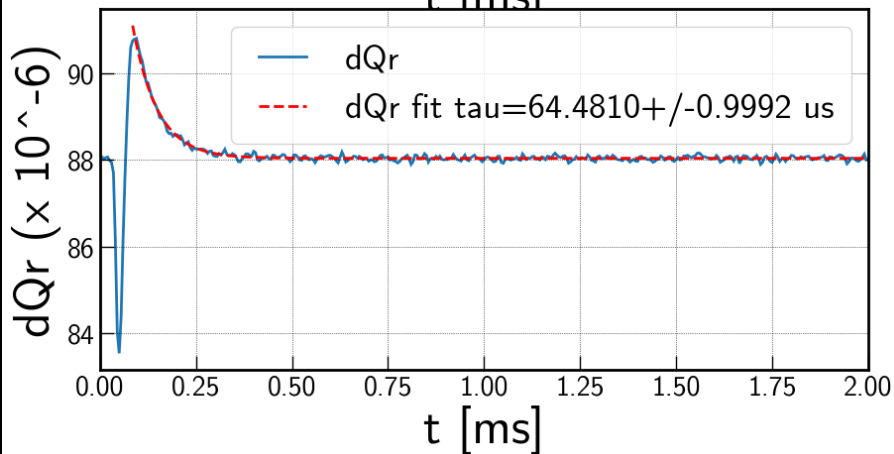
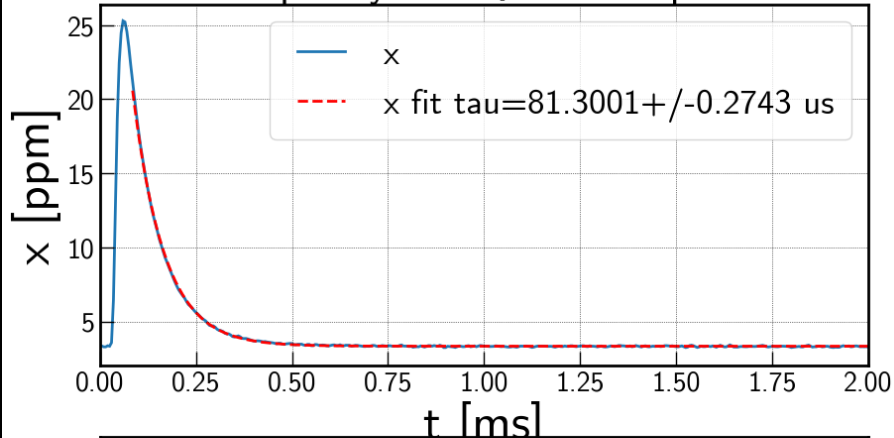
Stacked timestreams of a released device during glitches in an unreleased device

Credit: Katie Hughes

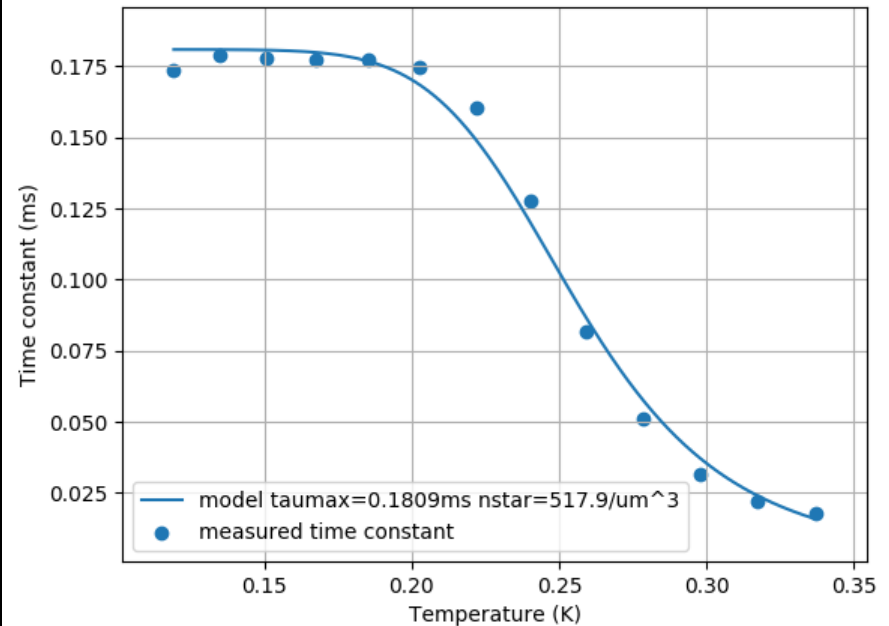


Quasiparticle Lifetimes

Frequency and Qr shift in pulse

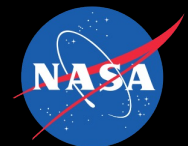


ch01 time constant vs temperature

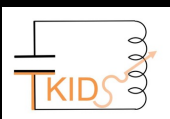


$$n^* = 517.9 \pm 40 / \mu m^3$$

$$\tau_{max} = 0.1809 \pm 0.0025 ms$$



Roger O'Brient



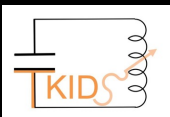
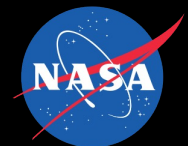
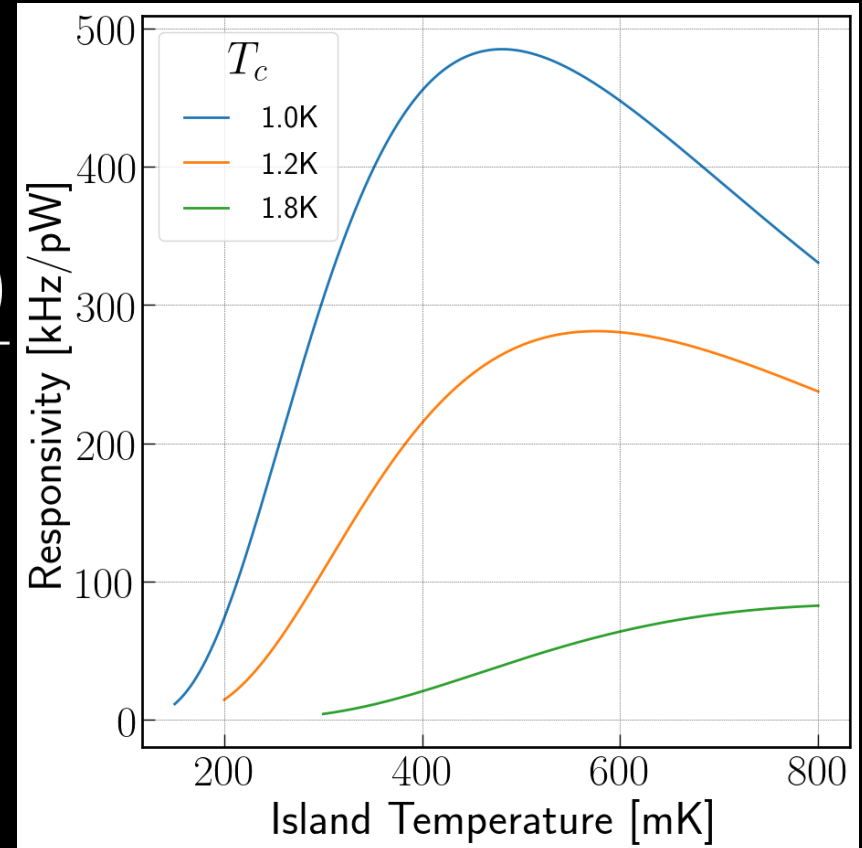
Responsivity Details

$$S = \frac{\partial f_r}{\partial P} = \frac{\partial f_r}{\partial n_{qp}} \frac{\partial n_{qp}}{\partial T} \frac{\partial T}{\partial P}$$

$$S = \frac{\partial f_r}{\partial P} = f_r(T) \frac{\beta(\omega, T) \kappa(T)}{2Q_i G(T) T}$$

$$\kappa(T) = \frac{1}{2} + \frac{\Delta}{k_B T}$$

$$\beta(f, T) = \frac{1 + \sqrt{\frac{2\Delta}{\pi k_B T} \exp\left[-\frac{hf}{2k_B T}\right]} I_0\left[\frac{hf}{2k_B T}\right]}{\frac{2}{\pi} \sqrt{\frac{2\Delta}{\pi k_B T} \sinh\left[\frac{hf}{2k_B T}\right]} K_0\left[\frac{hf}{2k_B T}\right]}$$



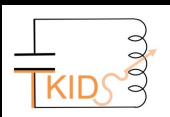
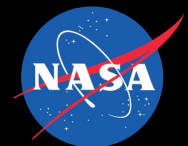
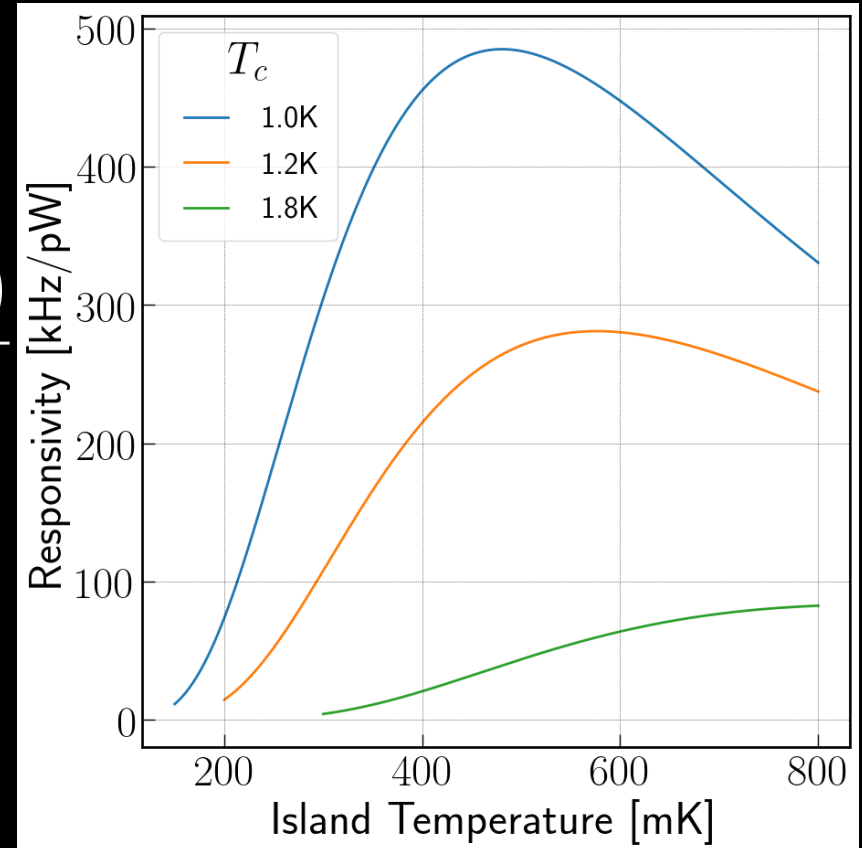
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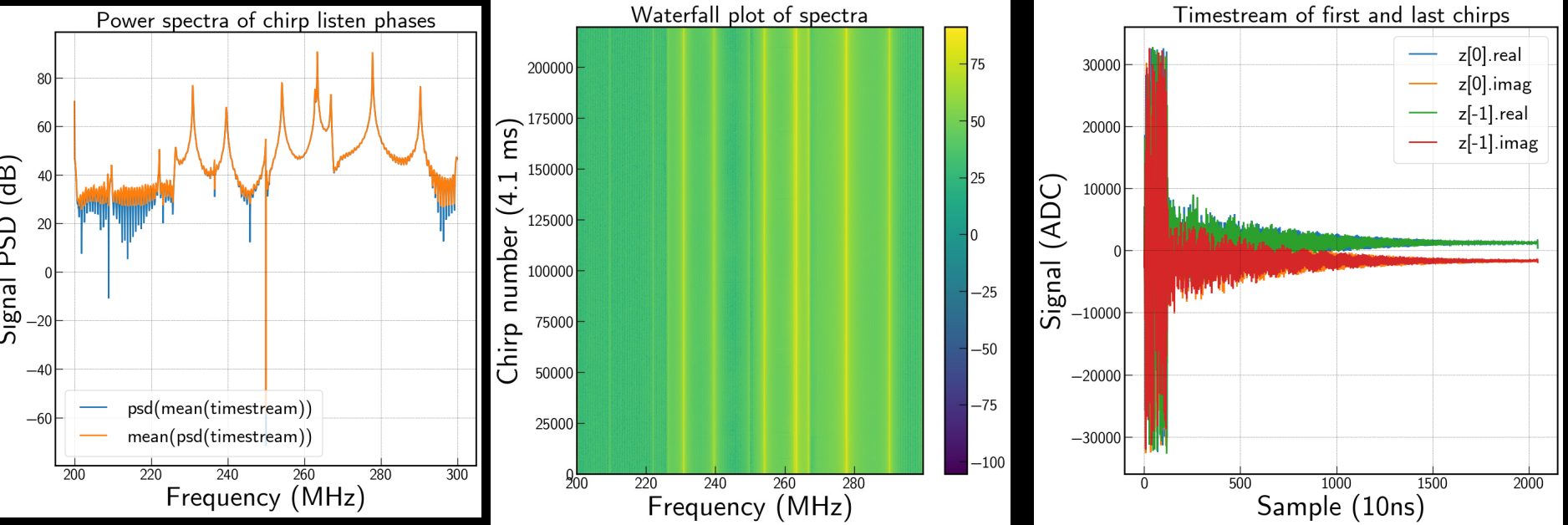
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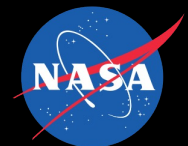
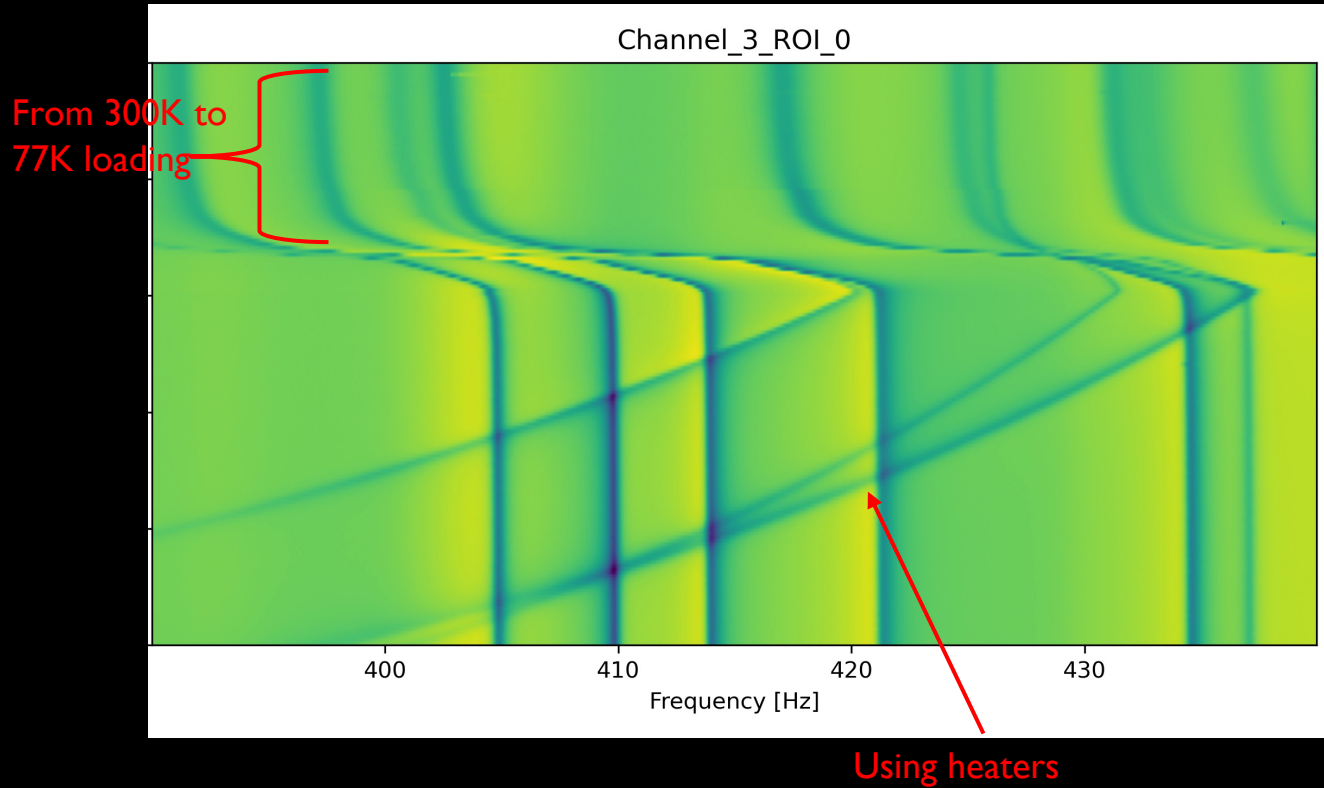


Chirped Readout

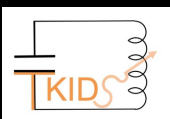


- Changes in optical loading during lab measurements shift the resonators by many line-widths
- In place of single-tone readout, we use a pulsed readout scheme
- Excite the resonators by applying a short chirp sweeping from high to low frequency
- Disable the transmit amplifier and listen to the resonator ringdown response.

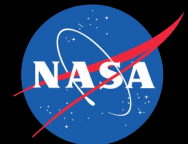
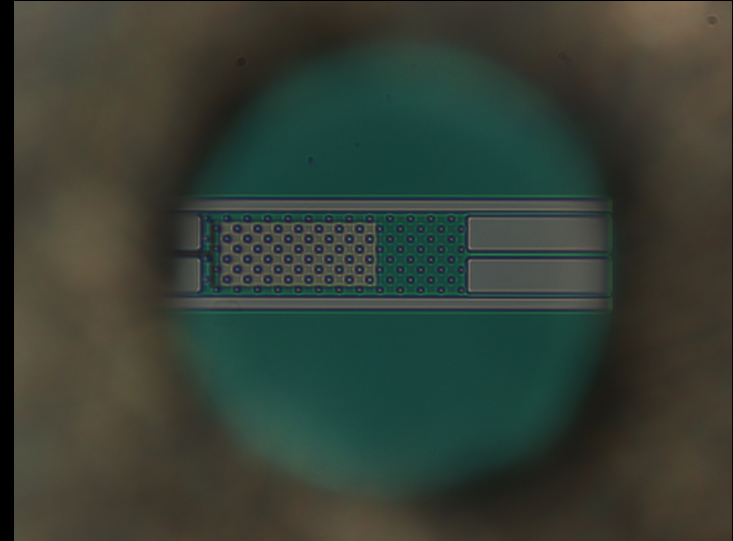
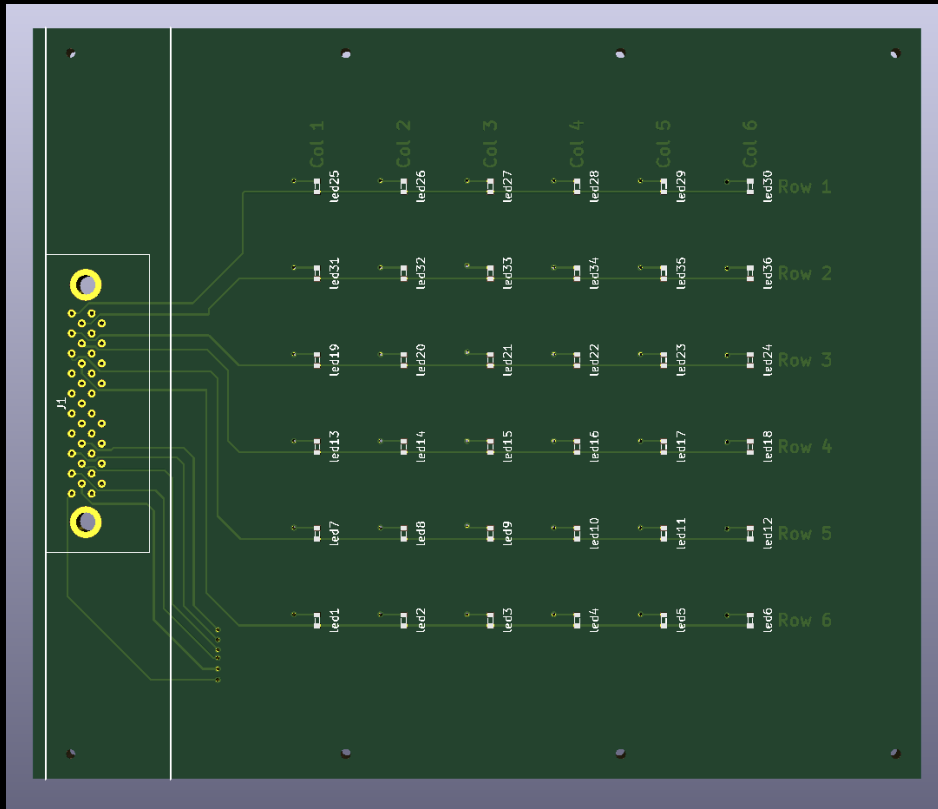
Chirped Readout



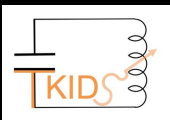
Roger O'Brient



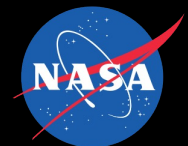
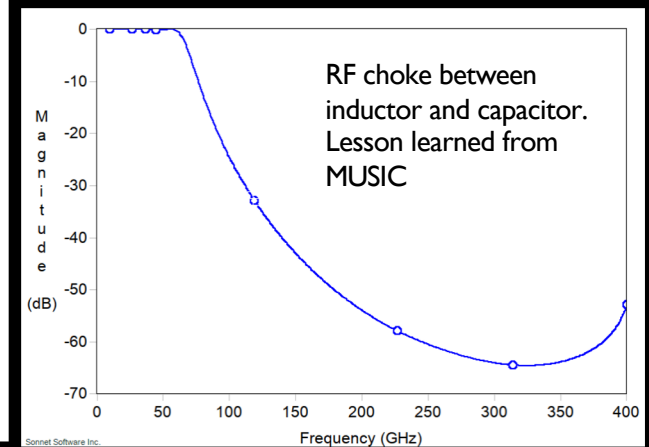
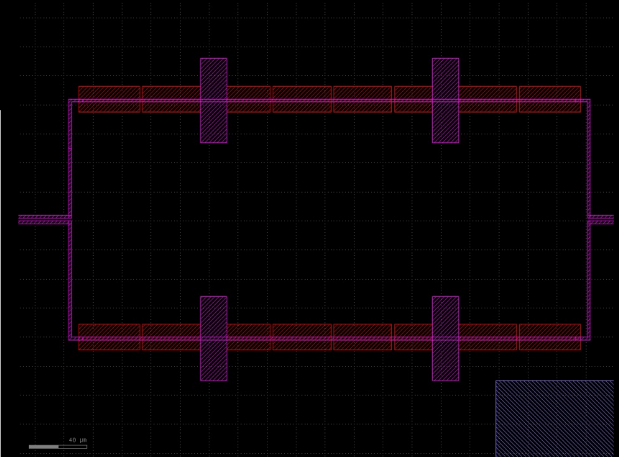
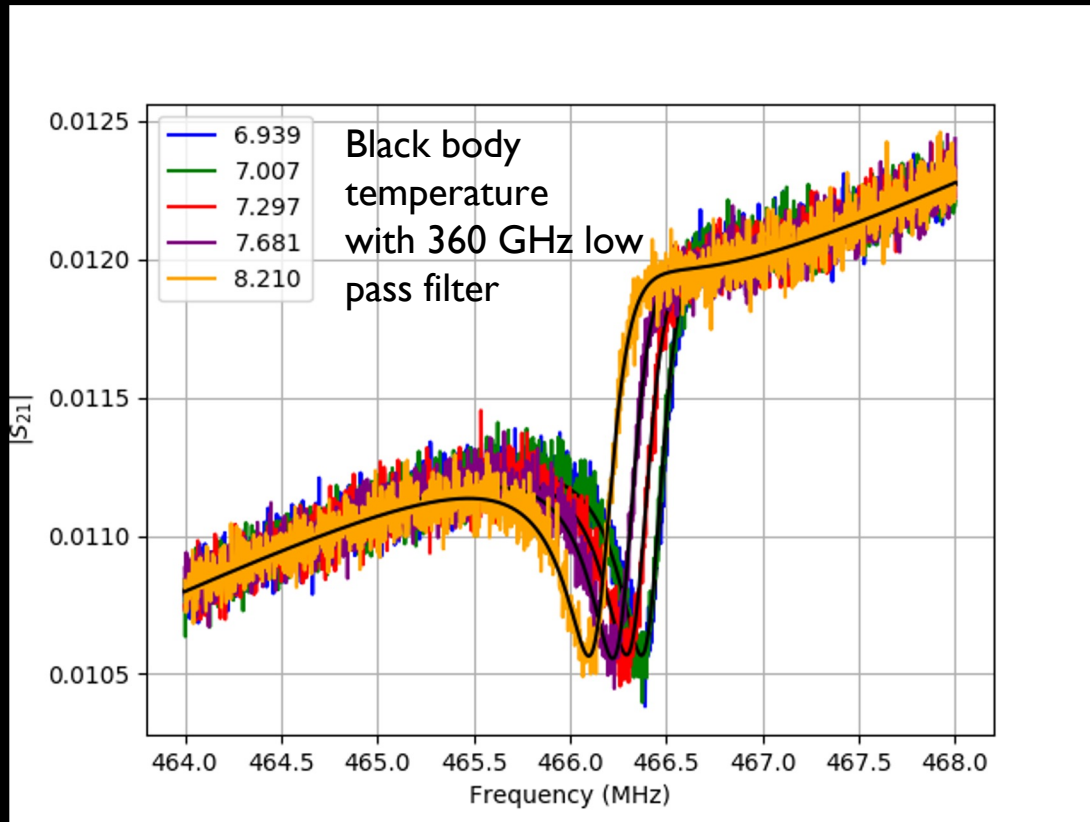
LiteBrite® Testing



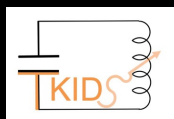
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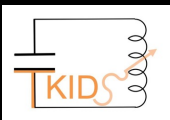
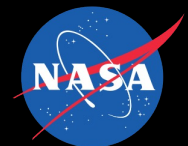
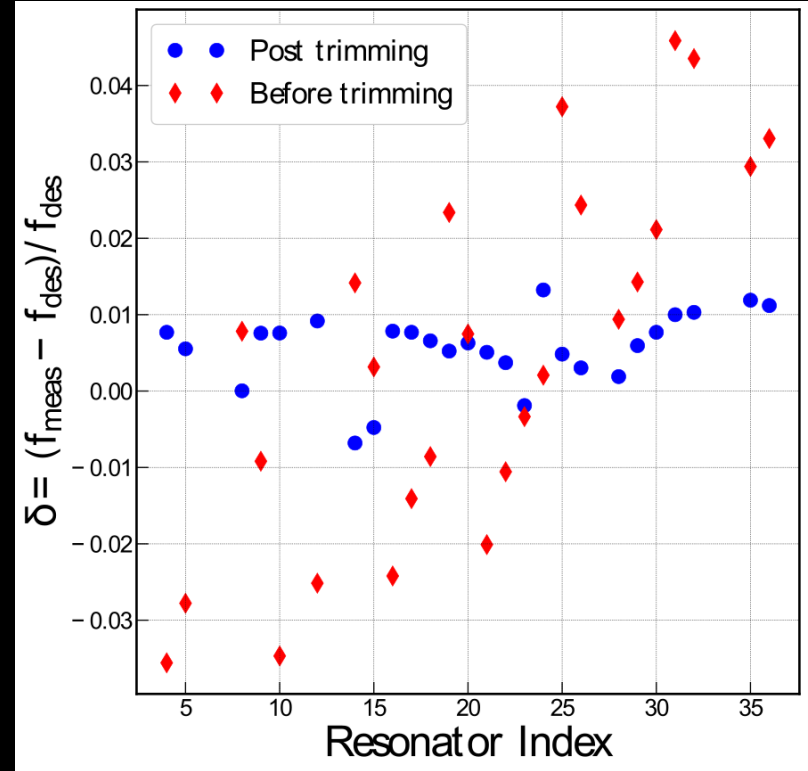
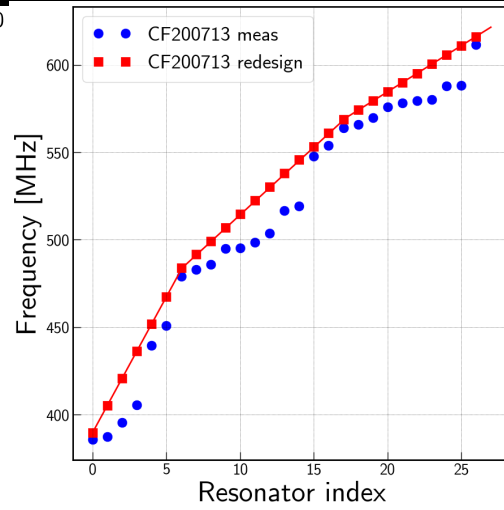
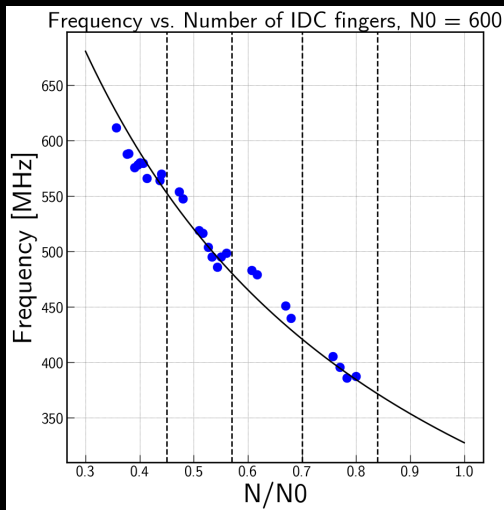
RF Choke



Roger O'Brient



Trimming Capacitors



Yield

- Best yield on TKID tile: 112/128 detector pairs
- Eliminated vias to GND in the design of the Antenna-Coupled TKID chips
- Have estimated defect density on capacitors through optical inspection: $0.299/\text{mm}^2 \pm 0.063$
- Feedline defects can be fatal.

