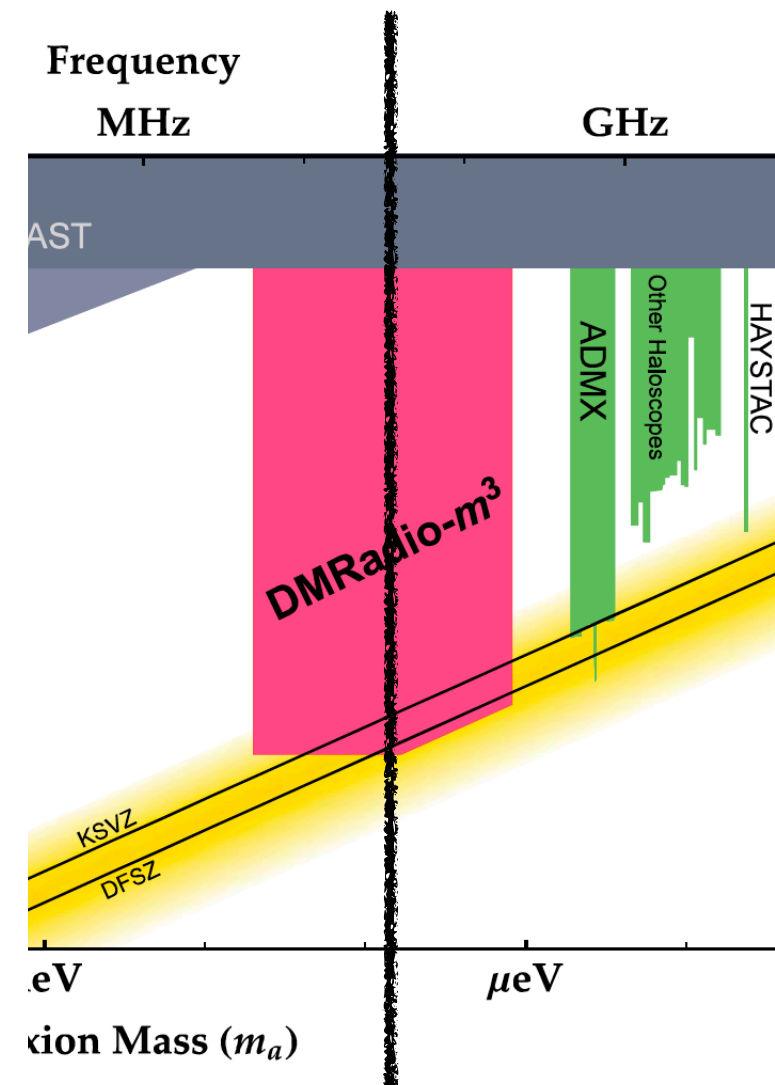


# DM Radio M<sup>3</sup> Coaxial Design

DM Radio Collaboration Meeting  
J. Singh — Stanford University  
13 August 2020

# Objectives

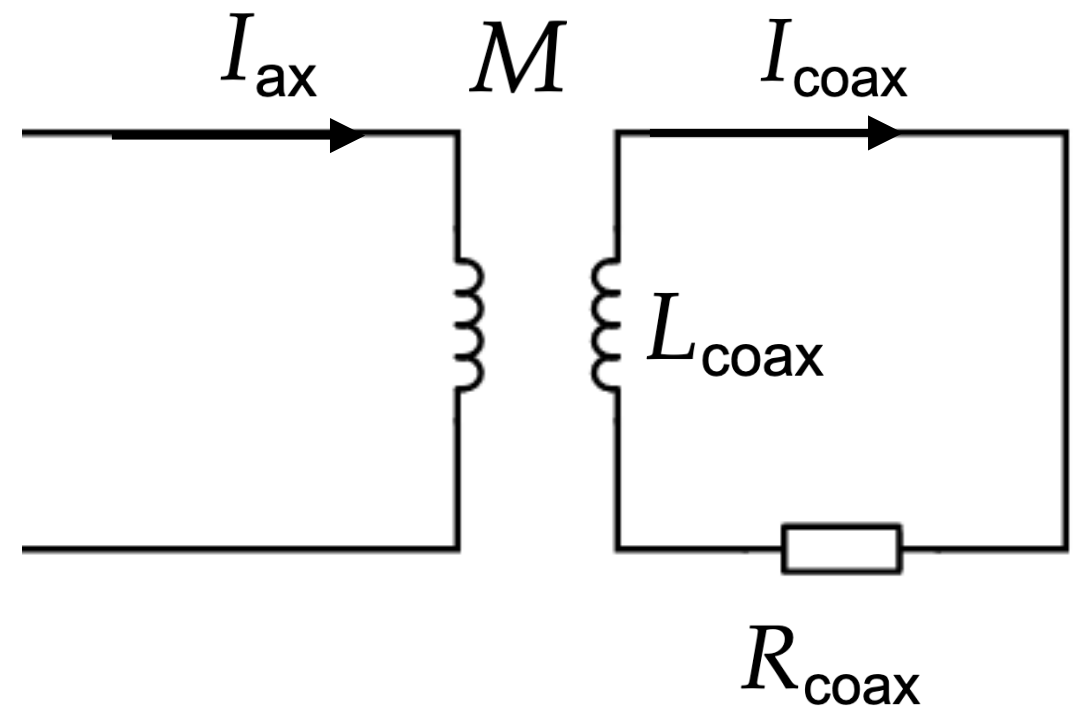
- Strawman design that couples coax to resonator.  
Assumptions:
  - **Quasistatic (30 MHz)**
  - **Pencil Limit**
  - **Homogenous B field in coaxial pickup**
- Evaluate FOM for coupled system to get sensitivity estimate:
  - Evaluate impact on coupled energy and Q.
  - Compare with performance required in proposal.



**30 MHz**

# Uncoupled Coax Circuit Model

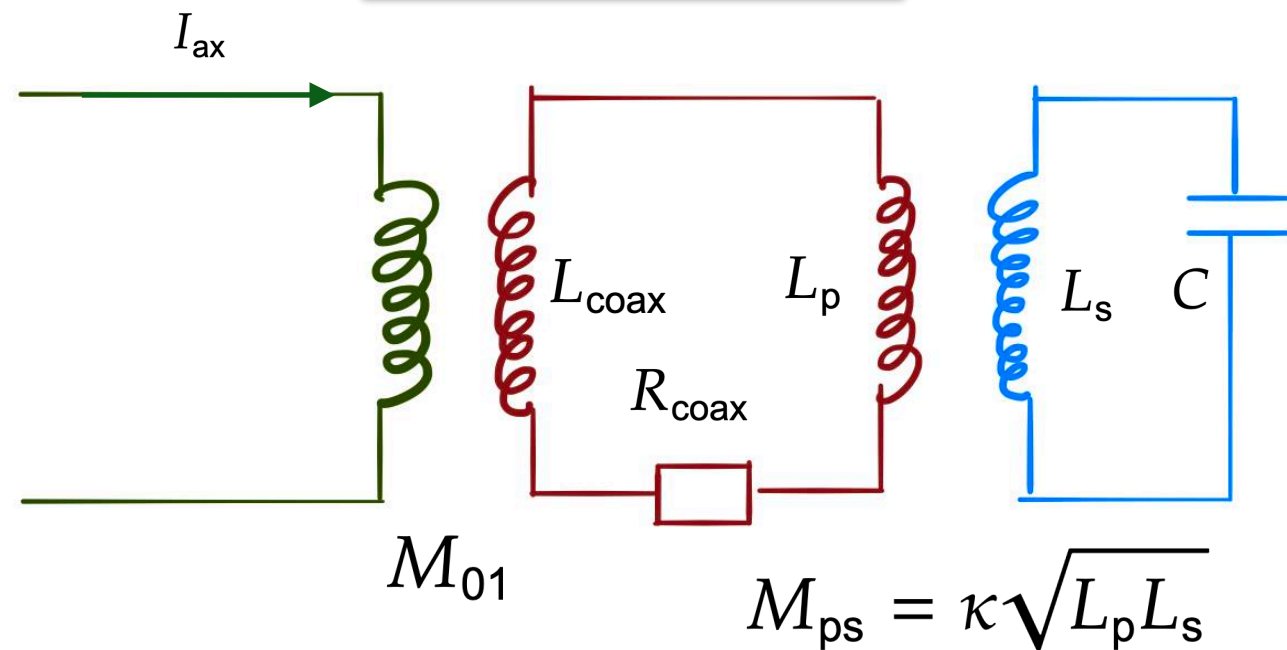
$$U_{\text{coupled}} = \frac{\phi_{\text{axion}}^2}{2L_{\text{coax}}} = \frac{(MI_{\text{ax}})^2}{2L_{\text{coax}}}$$



# Coupled Circuit Model

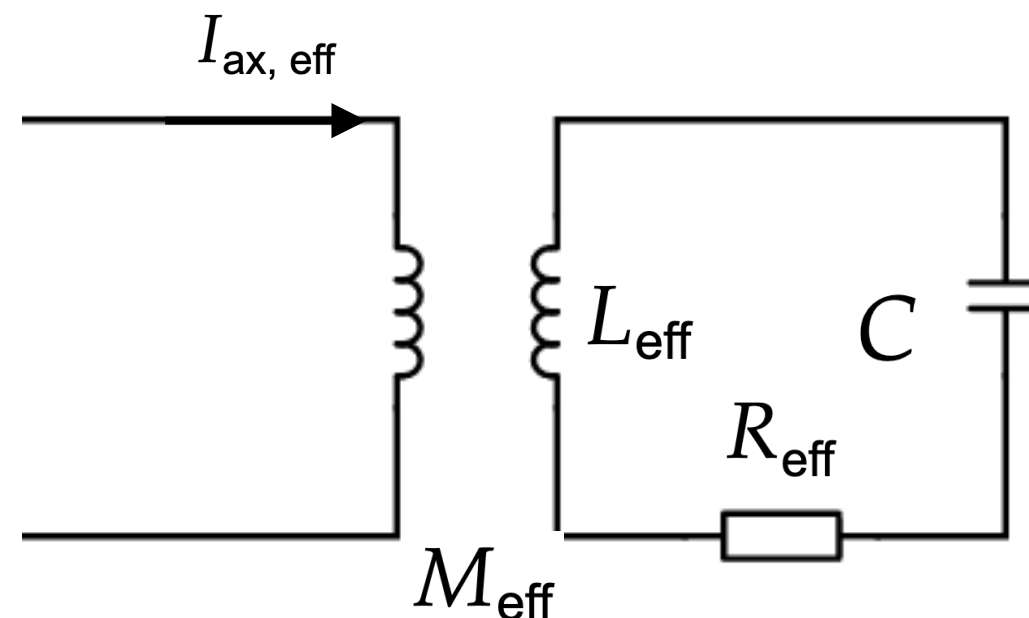
Coax

DM Input  
(Stiff Current)



Resonator  
(outside B field)

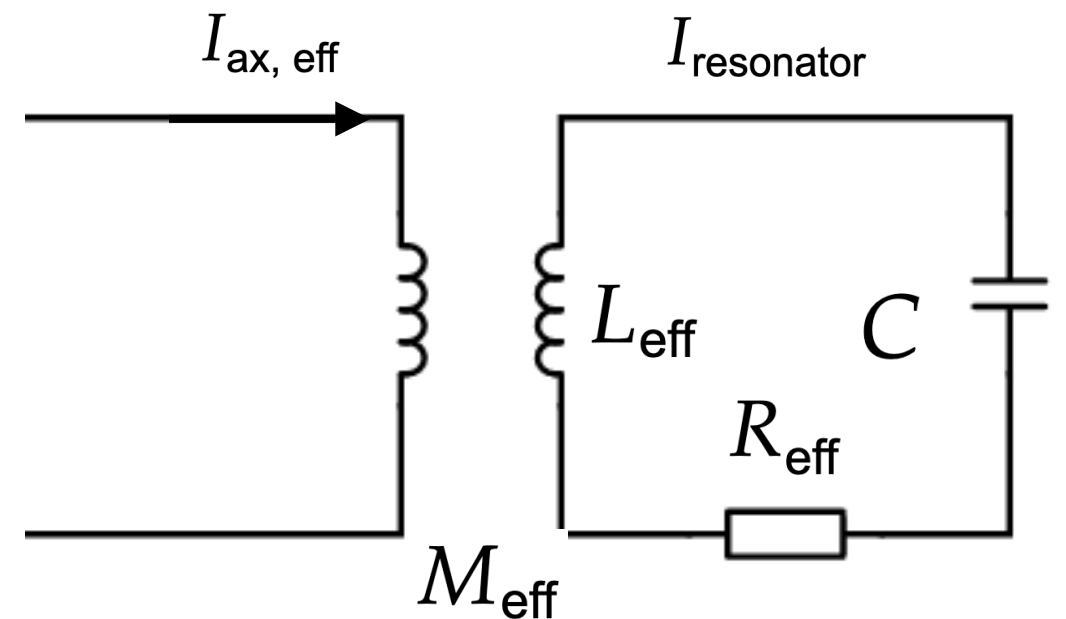
Effective Stiff  
Input Current  
 $I_{ax, eff}$



Effective  
(Resonator +  
Coax) Circuit

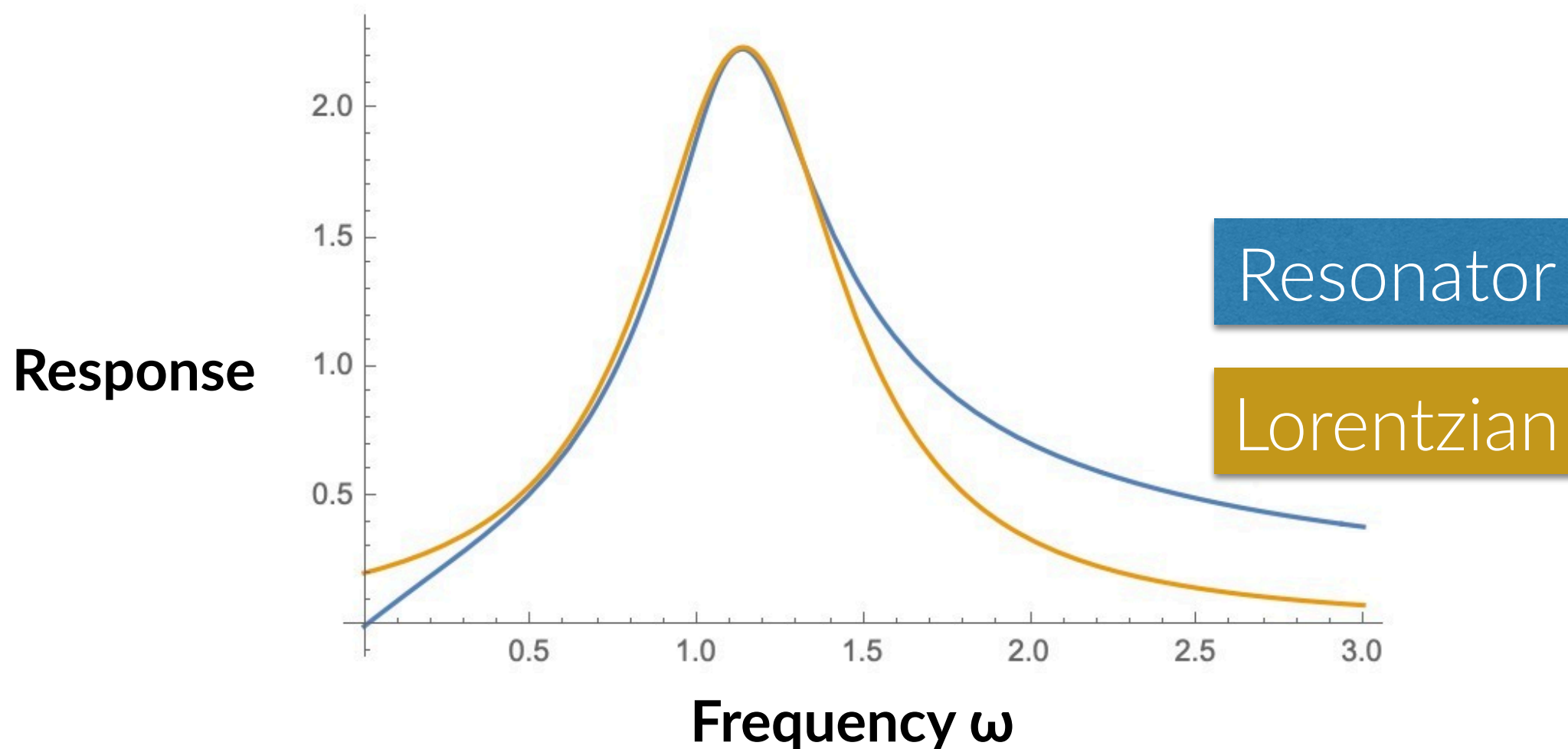
# Coupled Circuit Model

$$U_{\text{coupled}} = \frac{\phi_{\text{axion}}^2}{2L_{\text{eff}}} = \frac{(M_{\text{eff}} I_{\text{ax, eff}})^2}{2L_{\text{eff}}}$$



# Resonant Frequency & Q

- Effective circuit response with impedance  $Z = i\omega L_{\text{eff}} - i/\omega C + R$  is Lorentzian near resonance.



- Justifies expanding  $Z$  around resonant frequency to first order and approximating effective circuit as RLC resonator.

- Resonant frequency defined by minimum of  $\text{Im}(Z)$

$$\text{Im}(Z(\omega_0)) = 0$$

- Resonator parameters from Taylor Expansion.

$$Z(\omega) \approx R + 2iL(\omega - \omega_0)$$

- $Q$  from resonant frequency & Taylor Expansion.

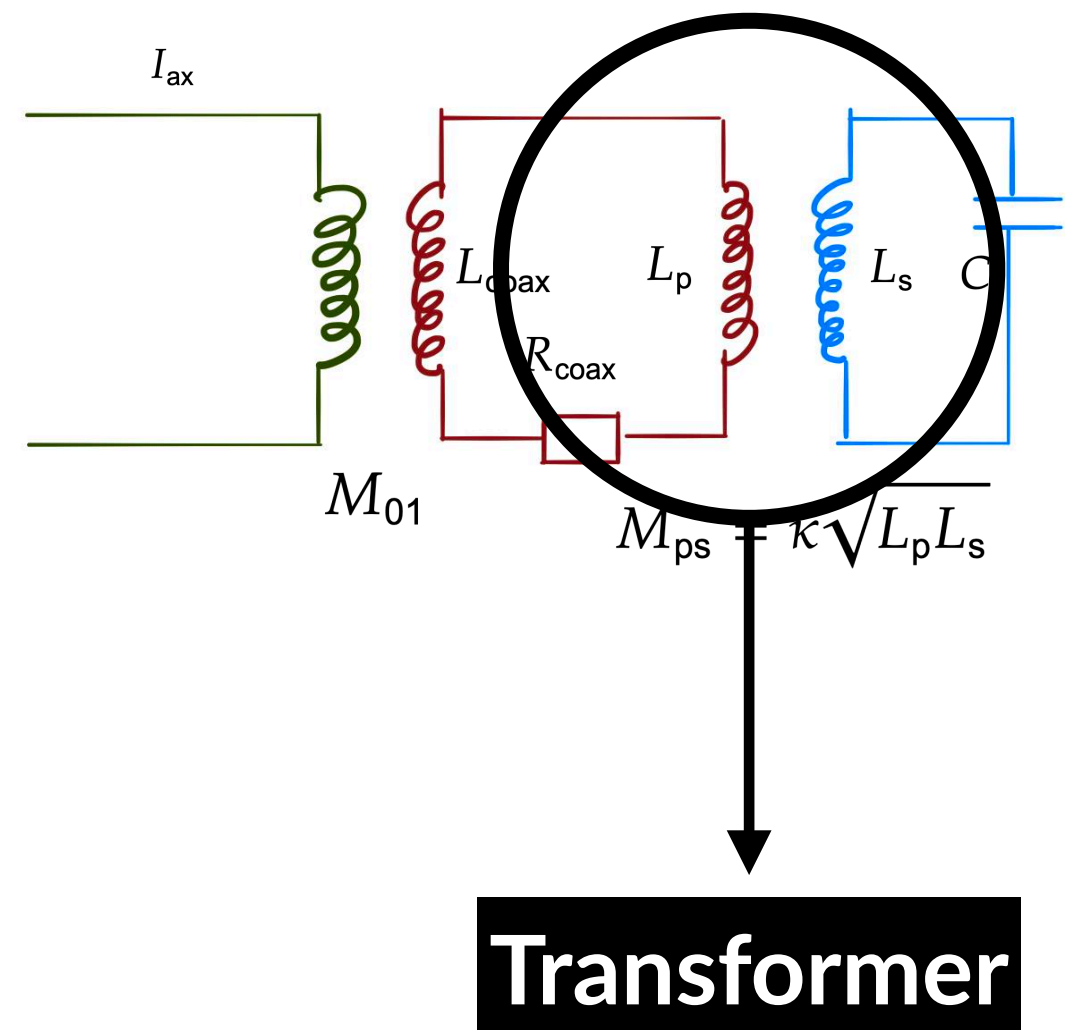
$$Q = \frac{\omega_0 L}{R}$$

- With  $Q$  and ratio of coupled energy, goal is to choose ‘good’ set of parameters which are physically reasonable.
- ‘Good’: degradation of  $Q$  & energy coupling that is tolerable vis-à-vis science goals.
- **WE DID NOT OPTIMISE FOR PARAMETERS**
  - Parameter values picked to give a *reasonable starting point* for further iteration.

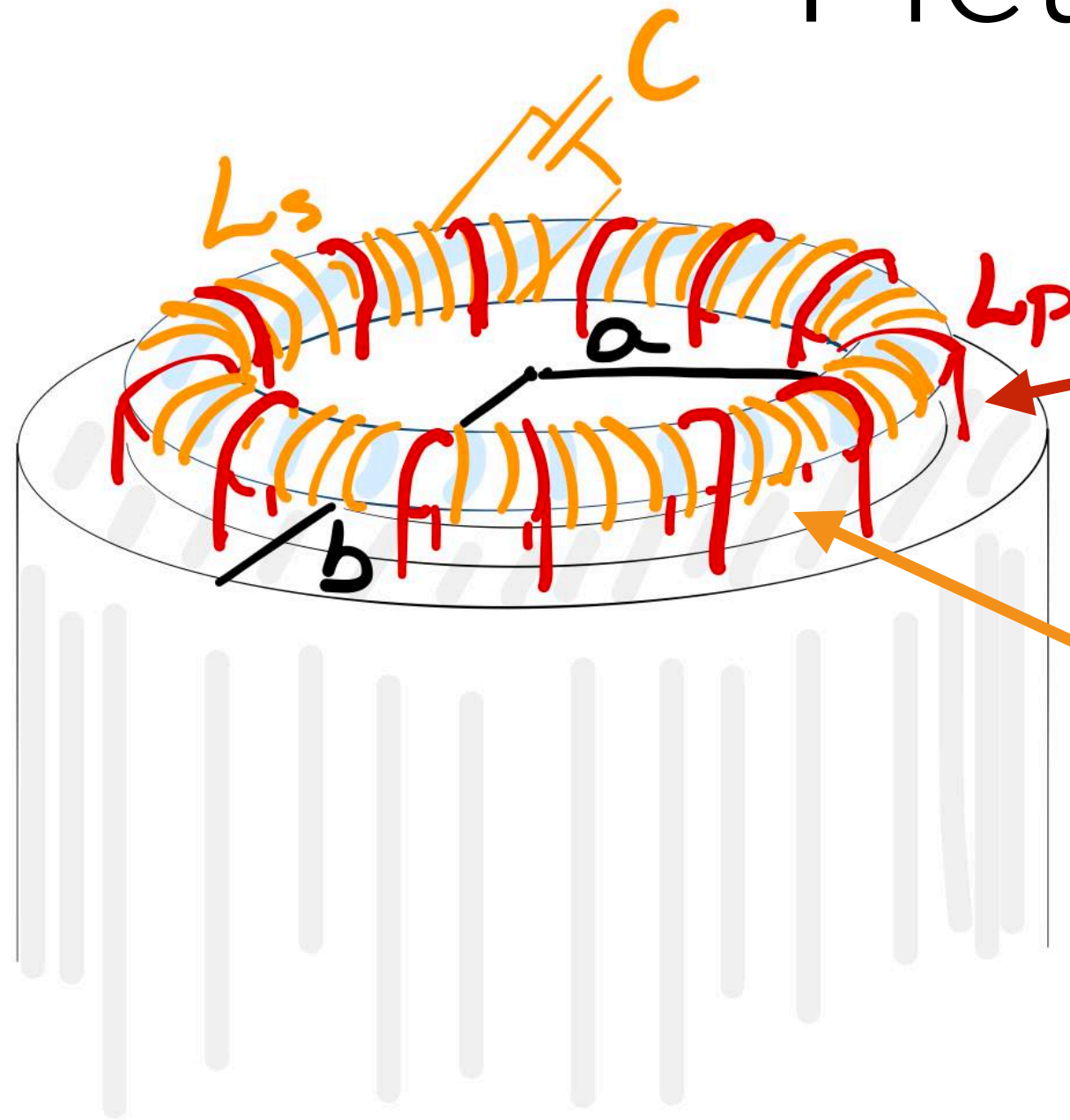


# Strawman Parameters

- Coax parameters:  **$a = 0.3\text{m}$ ,  $b = 0.68\text{m}$ ,  $h = 1.38\text{m}$**
- Transformer:
  - **$L_p = 0.2 \mu\text{H}$**
  - **$\kappa = 0.8$**
  - Wires in transformer assumed superconducting and lossless
- Resonator Parameters:  **$L_s = 0.35 \mu\text{H}$   $C = 100 \text{ pF}$**
- **$T = 100 \text{ mK}$ ,  $B = 4.5 \text{ T}$**
- **$f = 32 \text{ MHz}$ ,  $Q = 1.6 \times 10^6$**



# Picture



**Primary Coil:**  
Series of single wire loops ( $r=5\text{cm}$ )  
connected to the coax slit

**Secondary Coil:**  
Toroid circular x-section  $r = 5\text{cm}$   
Toroid radius =  $45\text{cm}$

Not to scale!

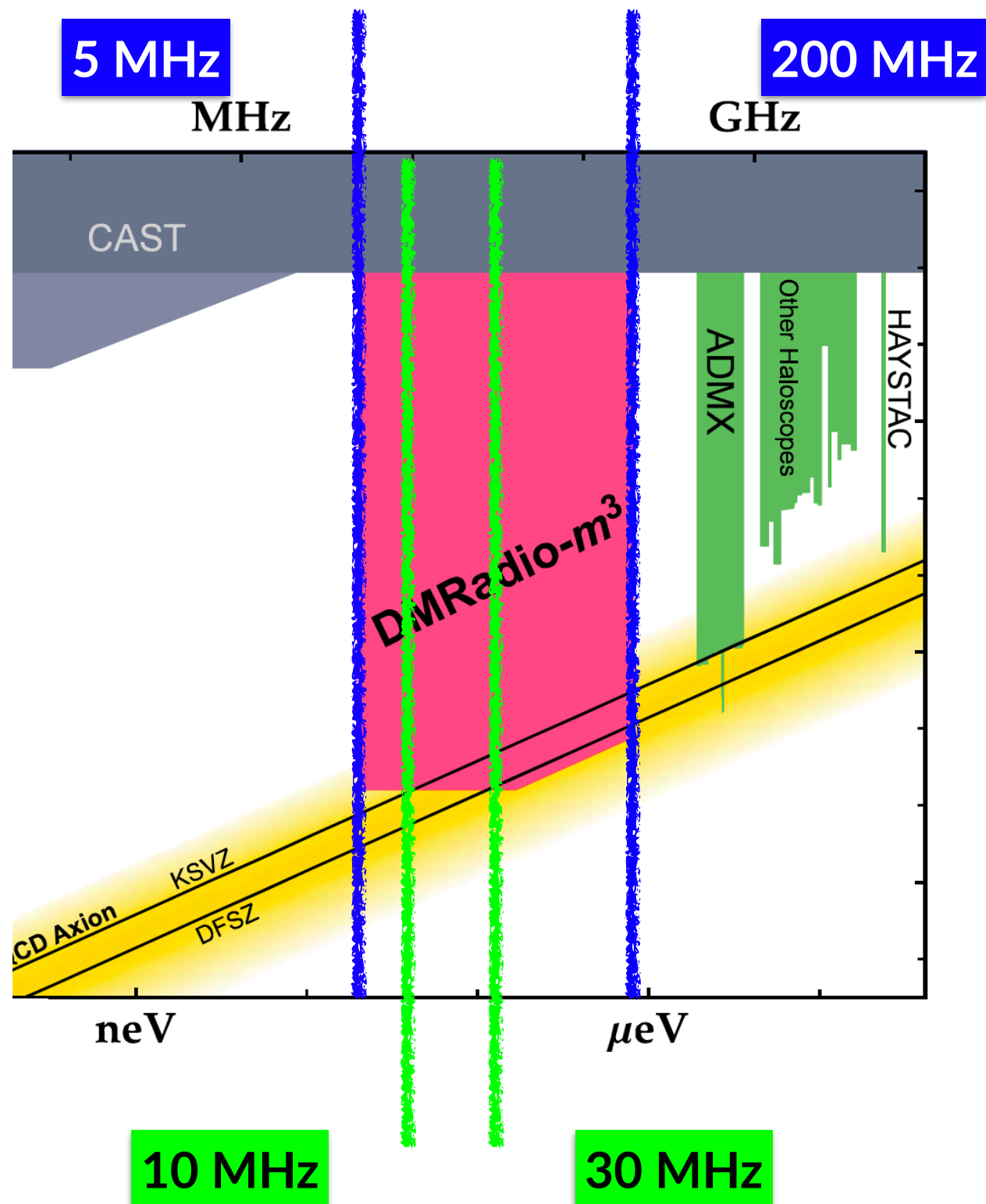
# Performance Estimate

- Transformer reduces coupled energy to 0.22× the original.
- Uncoupled coax Q:  $3.5 \times 10^5 \rightarrow$  Coupled Resonator Q:  $1.6 \times 10^6$ .
- Performance margin of -11%, i.e. underperforming vs. science goal.
- $B_0 = 4.5\text{T} \rightarrow B_0 = 5\text{T}$ : 0% margin, i.e. minimum for science goal, **plausible starting point.**

# Next Steps

- This straw man to be used for magnet design, get a real magnetic field profile.
- Refine inductance calculations beyond pencil using COMSOL etc.
- Components of a possible modeling campaign:
  - Coax inductance simulations
  - Transformer — what  $L_p$ ,  $L_s$  optimise energy transfer, what geometric constraints limit  $\kappa$ ?
  - Resonator — need as high  $Q$  as possible
  - A different coupling mechanism??

# Summary



**Coax Pickup:**  
 Material: Cu,  
 $\sigma = 6 \times 10^7 \text{ Sm}^{-1}$  (293K)  
 $a = 0.3\text{m}$   
 $b = 0.68\text{m}$   
 $h = 1.38\text{m}$   
 $V = 2\text{m}^3$   
 $B_0 = 5\text{T}$

**Transformer:**  
 $L_{\text{primary}} = 0.2 \mu\text{H}$   
 $L_{\text{secondary}} = 0.35 \mu\text{H}$   
 $K = 0.8$

**Resonator:**  
 $L_{\text{secondary}} = 0.35 \mu\text{H}$   
 $C = 100 \text{ pF}$   
 $f = 32\text{MHz}$   
 $Q = 1.6 \times 10^6$