

Straw Tube

Charlie Young



From APS Meeting @ Denver

Wire tension countered by tube wall

Successful assembly of one tube



**Tube
collapses if
the wire
tension is too
high!**

Gravitational Sag

Gravitational sag of wire is given by $\delta = \frac{(\rho\pi a^2)gL^2}{8T}$

where

ρ is density of wire material

a is wire radius

g is gravitational constant

L is wire length

T is tension force

Assuming

- 100 gm force = 0.981 Newton
- 50 μm diameter
- Density = 19.3 gm/cm³ (Tungsten)

Gravitation sag $\sim 75 \mu\text{m}$ for $L = 4 \text{ m}$

Electrostatic Deflection

Deflection at mid-point is given by $\delta = \frac{(\rho\pi a^2)g}{k_e} \left[\frac{1}{\cosh(\lambda L/2)} - 1 \right]$

where

ρ is density of wire material

a is wire radius

g is gravitational constant

k_e is a spring constant per unit length given by $k_e = \frac{\pi\epsilon_0 V^2}{R^2[\ln(R/a)]^2}$

R is tube radius

V is voltage

T is tension force

$\lambda = k_e/T$

Assuming

- 100 gm force = 0.981 Newton
- 50 μm diameter wire
- Density = 19.3 gm/cm³ (Tungsten)
- 1 cm radius tube
- 2 KV

Additional deflection $\sim 4 \mu\text{m}$ for $L = 4 \text{ m}$

Euler Buckling

Minimum cylinder thickness given by: $t_{min}^{Euler} = \frac{F(KL)^2}{\pi^3 ER^3}$

where

t is cylinder thickness

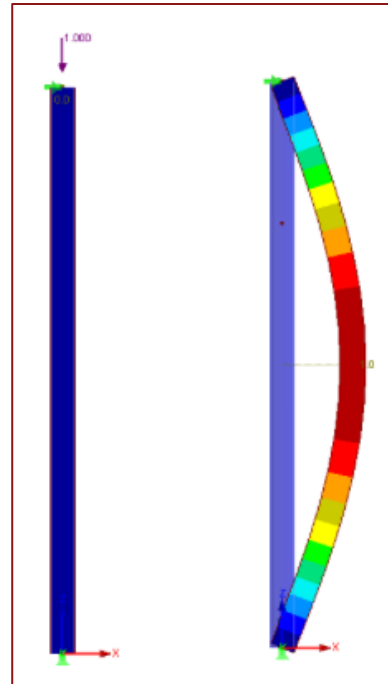
F is axial loading force

K is a scale factor for different endpoint constraints

L is cylinder length

E is Young's modulus of column material

R is radius of cylinder



Assuming

- 100 gm force = 0.981 Newton
- $K = 1$ (rotation-free translation-fixed constraints both ends)
- 4 m length
- 1 cm radius
- $E = 4$ GPa (Mylar)

Minimum thickness $\sim 185 \mu\text{m}$
Vs short prototype $\sim 12 \mu\text{m}$
(Safety factor not included)

Effective Length

$$L_{eff} = KL$$



Buckled shape of column shown by dashed line						
Theoretical K value	0.5	0.7	1.0	1.0	2.0	2.0
Recommended design value K	0.65	0.80	1.2	1.0	2.10	2.0
End condition key					Rotation fixed and translation fixed Rotation free and translation fixed Rotation fixed and translation free Rotation free and translation free	

Shell (Lorenz-Timoshenko) Buckling

Minimum cylinder thickness given by: $t_{min}^{shell} \approx \sqrt{\frac{FK}{0.61 \times 2\pi E}}$

Where

t is cylinder thickness

F is axial loading force

K is a scale factor for different endpoint constraints

L is cylinder length

E is Young's modulus of column material

R is radius of cylinder



Assuming

- 100 gm force = 0.981 Newton
- $K = 1$ (rotation-free translation-fixed constraints both ends)
- 4 m length
- 1 cm radius
- $E = 4$ GPa (Mylar)

Minimum wall thickness $\sim 10 \mu\text{m}$
(Safety factor not included. Large factor for extreme thickness to length ratio)

Transverse Momentum Resolution

IDEA-like layout

```
# IDEA
#
# beam pipe
# thickness from https://repository.cern/records/p44x1-18z28 Table 2
# position per email from Fabrizio Palla
0.0061 1.0e+3 1.0e+3 0.015
#
# vertex detector
# thickness per email from Franco Bedeschi and https://arxiv.org/pdf/2502.21223
# hit resolutions per email from Franco and Fabrizio Palla
# position from above paper
0.0030 3.0e-6 3.0e-6 0.0137
0.0030 3.0e-6 3.0e-6 0.0237
0.0030 3.0e-6 3.0e-6 0.0348
0.0040 7.0e-6 7.0e-6 0.130
0.0040 7.0e-6 7.0e-6 0.315
#
# Vertex detector support tube
# thickness per email from Manuella Boscolo
# position is chosen randomly between last vertex layer and drift chamber inner wall
0.008 1.0E+3 1.0E+3 0.340
# drift chamber inner wall
0.0008 1.0E+3 1.0E+3 0.350
# drift chamber volume
1.03E-05 1.00E-04 2.00E-03 0.365
1.03E-05 1.00E-04 2.00E-03 0.379
1.03E-05 1.00E-04 2.00E-03 0.394
1.03E-05 1.00E-04 2.00E-03 0.408
1.03E-05 1.00E-04 2.00E-03 1.956
1.03E-05 1.00E-04 2.00E-03 1.971
1.03E-05 1.00E-04 2.00E-03 1.985
# drift chamber outer wall
0.012 1.0E+3 1.0E+3 2.00
#
# silicon wrapper -
# hit resolution per email from Franco
0.007 7.0E-6 9.0E-5 2.04
0.007 7.0E-6 9.0E-5 2.08
```

112 drift chamber layers

- The four numbers in each detector plane are:
 - Thickness (X0)
 - R-phi hit resolution (m)
 - Z hit resolution (m)
 - Radial position (m)
- Hit resolutions set to 10^3 m for non-measurement planes such as support tube.

Transverse Momentum Resolution

straw-like layout

Remove drift chamber inner and outer walls
Change thickness to $1.32\text{E-}04 \times 0$ for $12\text{-}\mu\text{m}$ Mylar straw
Everything else unchanged

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0.0030 3.0e-6 3.0e-6 0.0348
0.0040 7.0e-6 7.0e-6 0.130
0.0040 7.0e-6 7.0e-6 0.315
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112 drift chamber layers

The four numbers in each detector plane are:

- Thickness ($X0$)
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- Z hit resolution (m)
- Radial position (m)

Hit resolutions set to 10^3 m for non-measurement planes such as support tube.

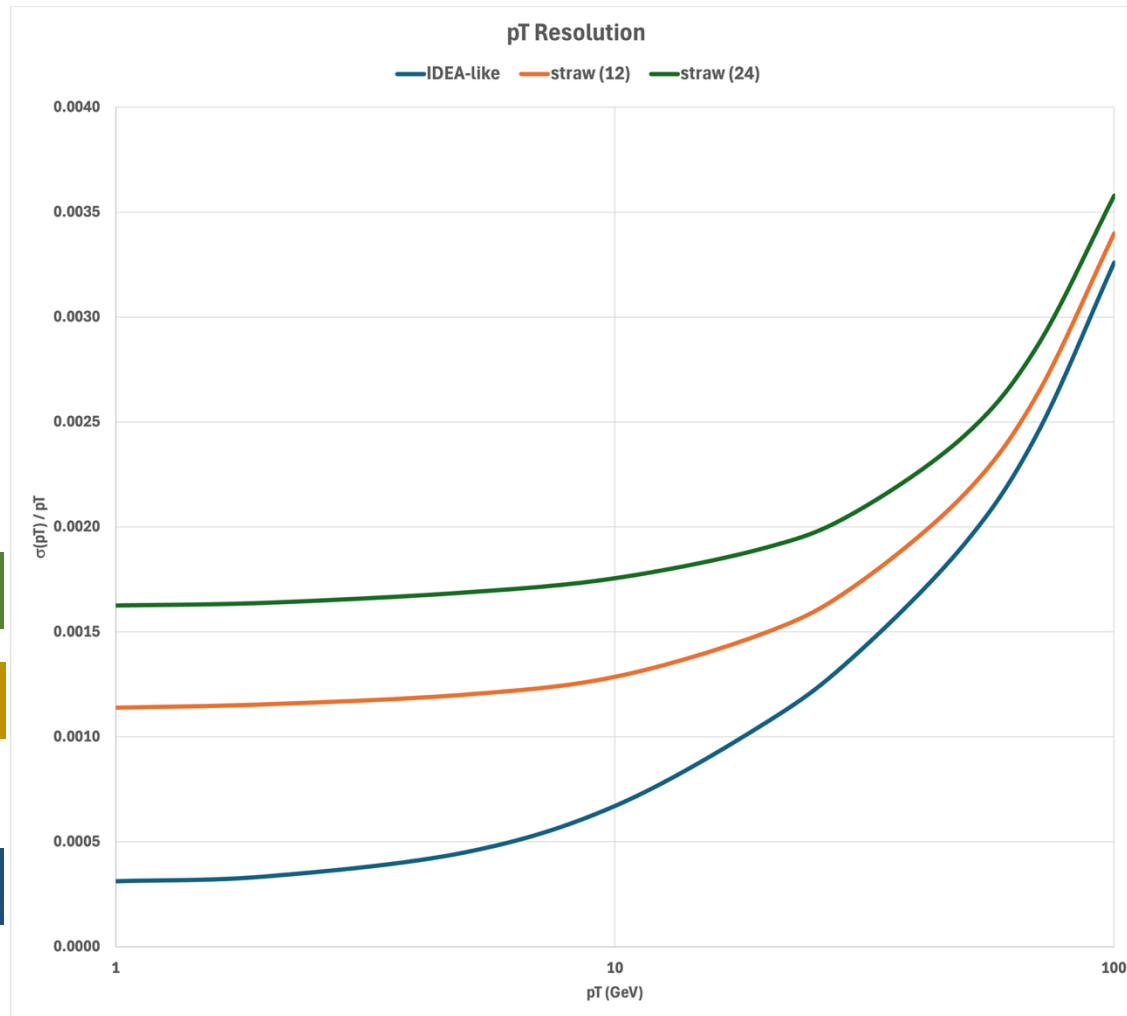
Transverse Momentum Resolution

<https://github.com/slaclab/TrackingResolution/tree/master>

Straw (24 μm)

Straw (12 μm)

IDEA



Transverse Momentum Resolution

IDEA-like layout w/o wrapper

Remove silicon wrapper
Everything else unchanged

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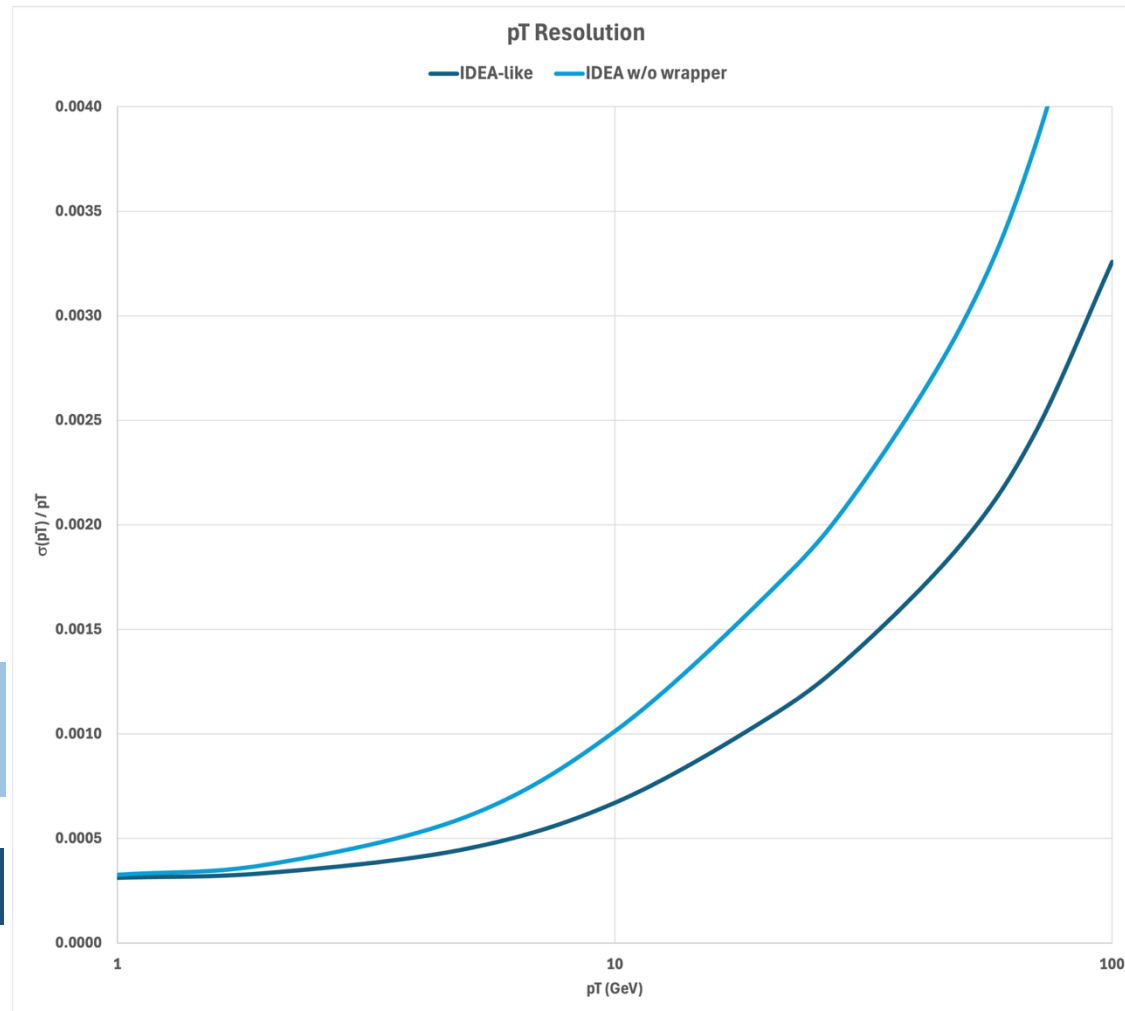
Hit resolutions set to 10^3 m for non-measurement planes such as support tube.

Transverse Momentum Resolution

<https://github.com/slaclab/TrackingResolution/tree/master>

IDEA w/o wrapper

IDEA



Conclusion

Straw tube with 12- μm thick walls (default)

- $\sigma(pT) / pT \sim 0.001$ at low momentum, approximately 3x worse than IDEA
- Far exceeds buckling limit from wire tension

Options:

- Thicker tube walls but even worse momentum resolution
- Transfer load to external support
 - Still need to thin down straw tubes for competitive resolution

Silicon wrapper crucial for high-momentum performance