



Solid State RF Amplifier Development for 805 MHz Klystron Replacement at LANSCE

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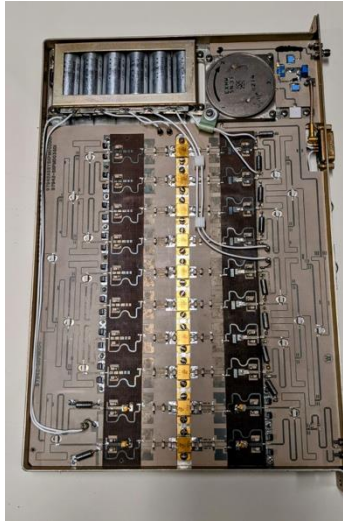


Forty-four Klystrons used for 805 MHz RF power for LANSCE Coupled-Cavity Linac

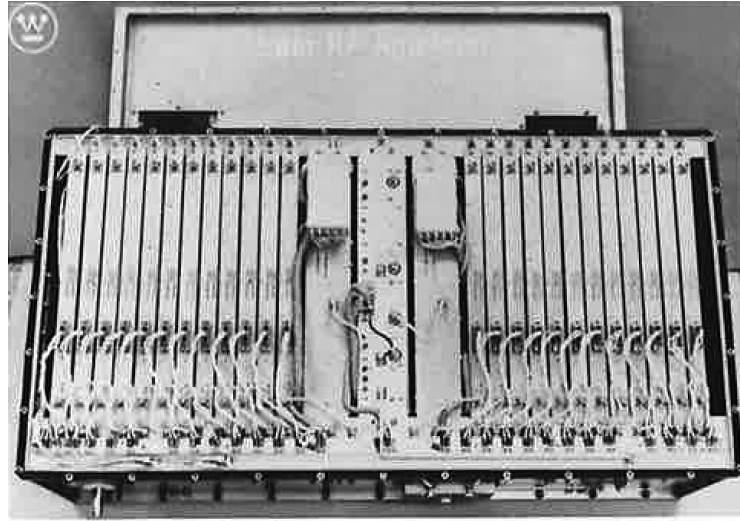


- 1.25 MWp, 150 kW average power, 1960s mod anode design
- Concerns of long term supply past 2050
- Beam HV systems obsolete
- 50+ year old technology is difficult to staff with early career engineers and technologists without lengthy training period (years)

In 1980s, LANL Collaborated with Industry on 2 x 60 kW SSA for Space Accelerator BEAR



2.5 kW module using
10 x 500 Watt BJT

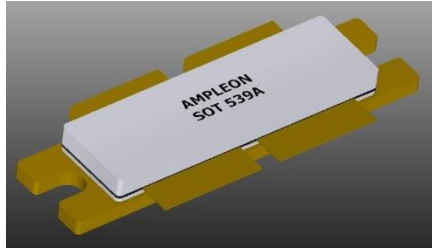


60 kW PA, 36 x 18 x 10 inches, 120 lbs

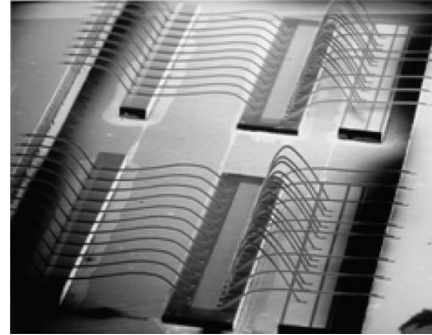


Launched July 1989 from White Sands Range

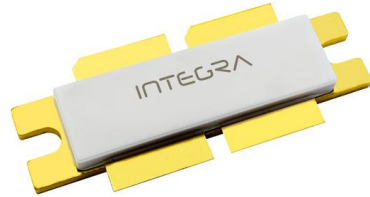
RF Power Transistors – Silicon LDMOS is Leader



- Below 400 MHz LDMOS ~ 1.8 kW P_{sat}
- Large transistor dies used for higher power have higher drain to source capacitance, reduced gain and efficiency, very low matching impedance
- 805 MHz power < 1 kW per transistor



Gallium Nitride on Silicon Carbide High Electron Mobility Transistor



- **Smaller structure with lower capacitance and highest power density**
- **Capable of higher temperature operation, up to 225 deg C internally**
- **Now able to generate 6-7 kW depending on voltage, up to L Band for avionics**

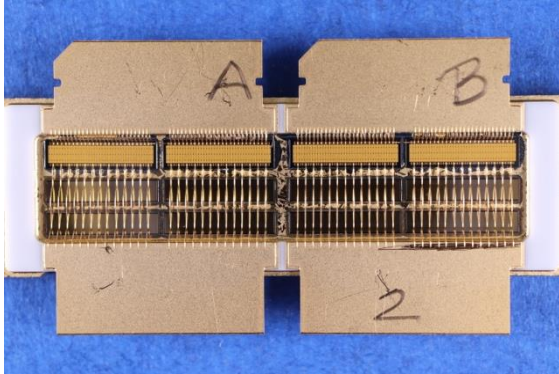
Gallium has 3 Valence Electrons, Nitrogen and Arsenic have 5

Material	GaN	Si	GaAs	SiC (4H)
Bandgap (eV)	3.4	1.1	1.4	3.2
Breakdown Field Strength (MV/cm)	2	0.3	0.4	2.2
Saturated Velocity (x10 ⁷ cm/s)	2.5	1	1.5	2
Thermal Conductivity (W/cm-K)	1.5	1.3	0.4	4

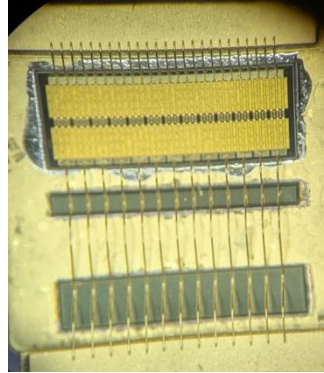
Our SSA is using GaN on SiC Transistor Technology

- 805 MHz with LDMOS required excessive devices (system must fit in Klystron space)
- Integra Technologies released HV GaN in 2022; long device production life is forecasted
- Navy is investing in very high power and bandwidth also
- They don't sell in the wireless market, so their production runs are smaller
- Collaborating with combiner company (Werlatone) for the blade design and overall combining architecture
- Third year of internal R&D, progress shown in following slides

IGN815 is Gen 3 HEMT



IGN815, 3.6 kWp, 12% duty Factor



IGN825, First die is mounted, 1/4 of 5 kWp, 12% duty Factor



- **Made from four inch GaN on SiC wafers from foundries**
- **4 x 0.25" wide transistor dies, each having 78 x 1 μm gate length, stable design**
- **78 mm gate periphery per die for 3.6 kWp, 117 mm for 5 kWp part**
- **Ag bond wires, AuSn soldered die attach to CPC flange**

IGN815 Preliminary Datasheet

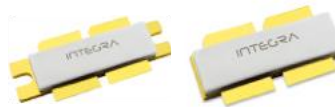
IGN815 | RF Power Transistor
IGN815S

INTEGRA
RF POWER DEVICES

UHF-Band, GaN/SiC, RF Power Transistor

805 MHz | 3600W | 75% Efficiency typ | 20 dB Gain typ | 100 V | 1ms Pulse Length, 12% Duty Cycle

IGN815 and IGN815S are high power GaN-on-SiC RF power transistors that have been designed to suit the unique needs of particle accelerator systems. They supply a minimum of 3600W of peak output power, with typically 20 dB of associated gain and 75 % efficiency. They operate from a 100V supply voltage. For optimal thermal efficiency, the transistors are housed in a metal-based package with an epoxy-sealed ceramic lid.



FEATURES

- GaN on SiC HEMT Technology
- Output Power >3600W
- Pre-matched Input Impedance
- High Efficiency - 75% typical
- 100% RF Tested under 1ms, 12% duty cycle pulse conditions
- RoHS and REACH Compliant

APPLICATIONS

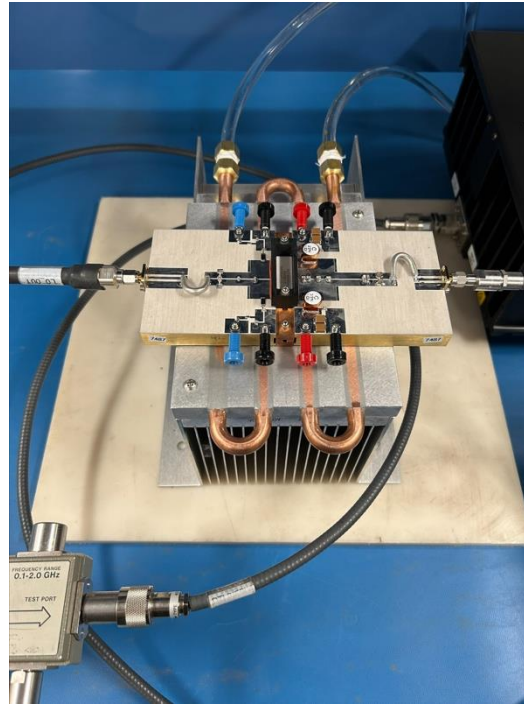
- Particle Accelerator Systems

Table 1. RF Electrical Characteristics (Case temperature = 30 °C unless otherwise stated)

Parameter	Symbol	Min	Typ	Max	Units	Test Conditions
Gain	G	16	20	24	dB	$P_{out} = 3600W$ $f = 805 MHz$ 1ms pulse length, 12% duty cycle $V_{GS} = 100V, I_{DS} = 75mA$ per side
Drain Efficiency	η	65	75	85	%	
Pulse Droop	D	0	-0.65	-0.8	dB	
Input Return Loss	IRL	7	15	18	dB	
VSWR Mismatch Stability	VSWR-S	2:1				
VSWR Withstand	VSWR-LMT	5:1				

Note: Consult Integra Technologies Application Note 001 for information on how RF output power and pulse droop are measured.

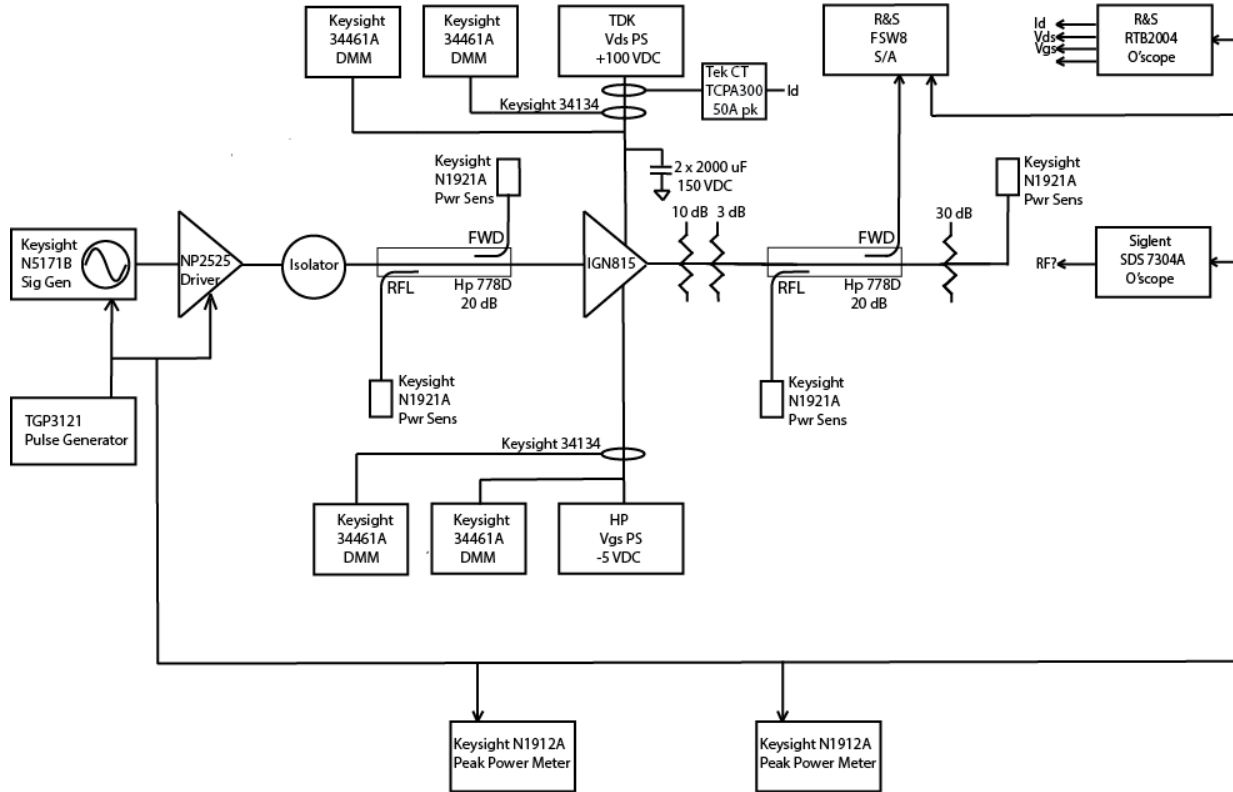
Push-Pull Test Pallet



3.6 kWp, 12% DF, 100 Volt Vds

185 deg C channel temp measured at factory

LANL Test Bench Diagram



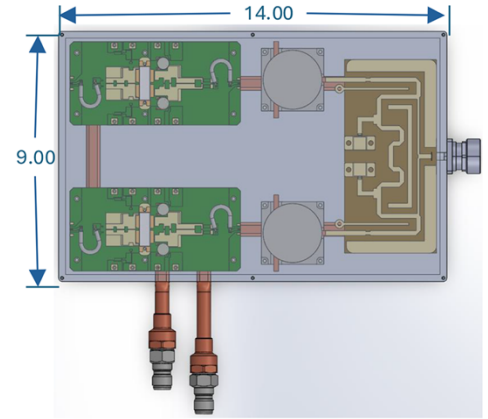
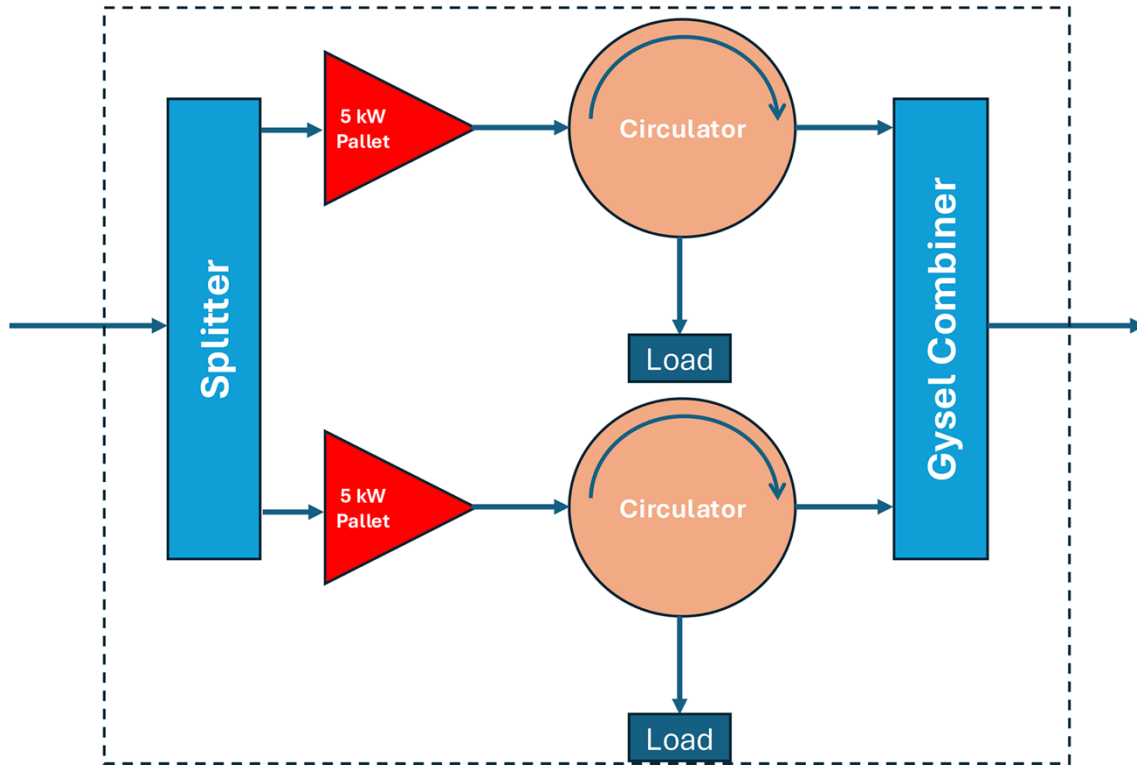
5 kWp 117 mm Periphery Chips are in Test at Fab

- Transistor chip development is $\sim 1/4$ cost of tube NRE
- Pizza mask from wafer lots, testing design variations
- Final chip selected, RF and thermal testing
- Packaged transistor development
- Tuning, measurement of RF parameters
- Final RF test fixture developed
- Pallet design and evaluation - first item test
- Takes about 1 year

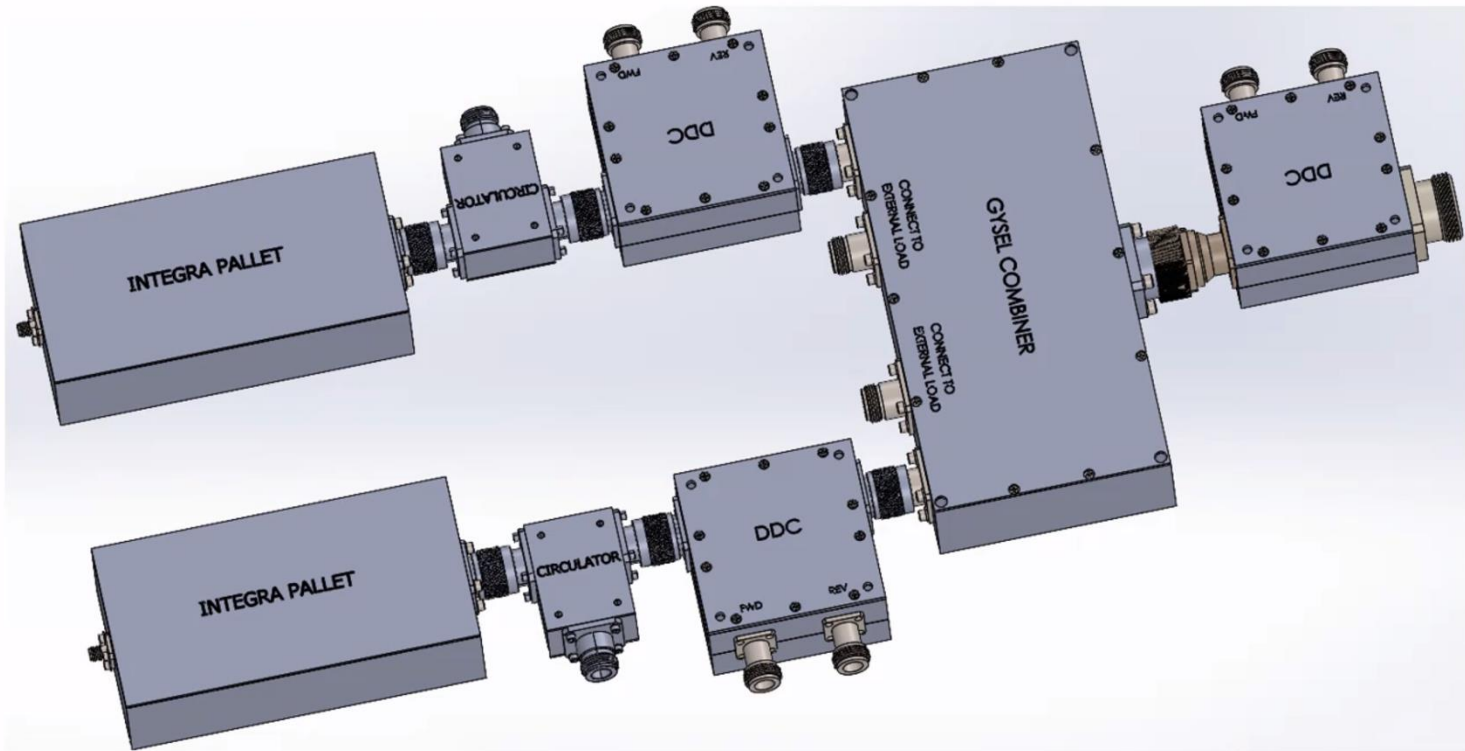
Combining Power Modules to get 1.25 MWp

“The rest of the story...”

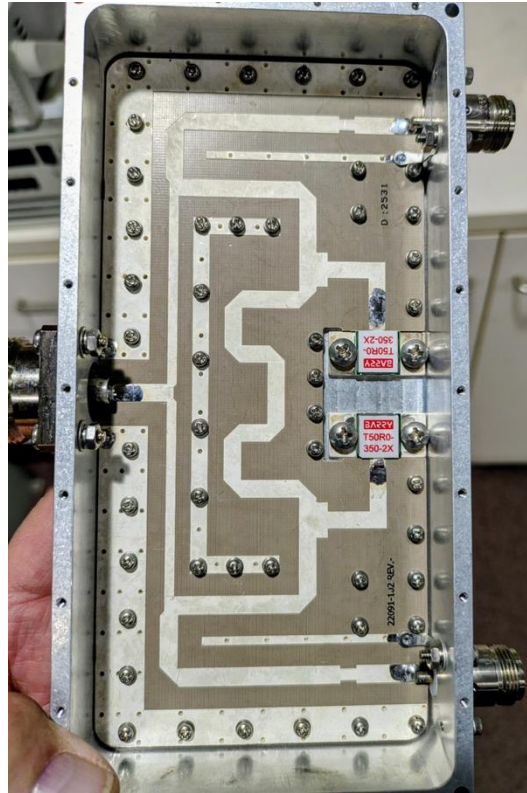
10 kWp Maximum for Blade due to Output Connector



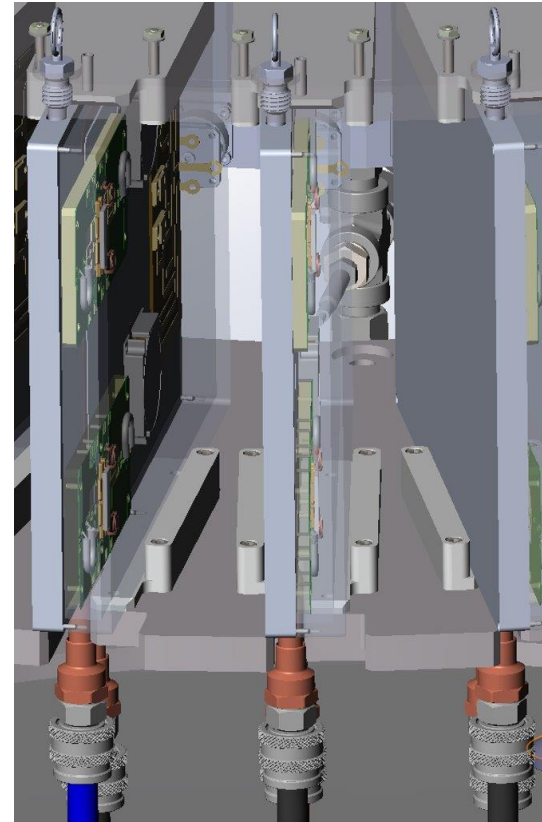
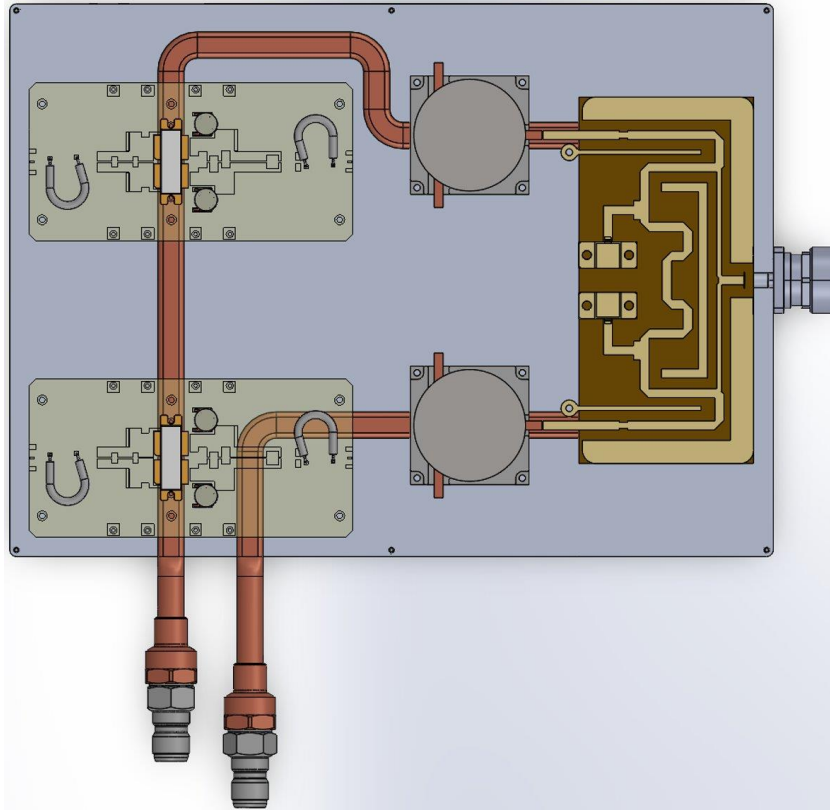
Benchtop Prototype of Components in Blade



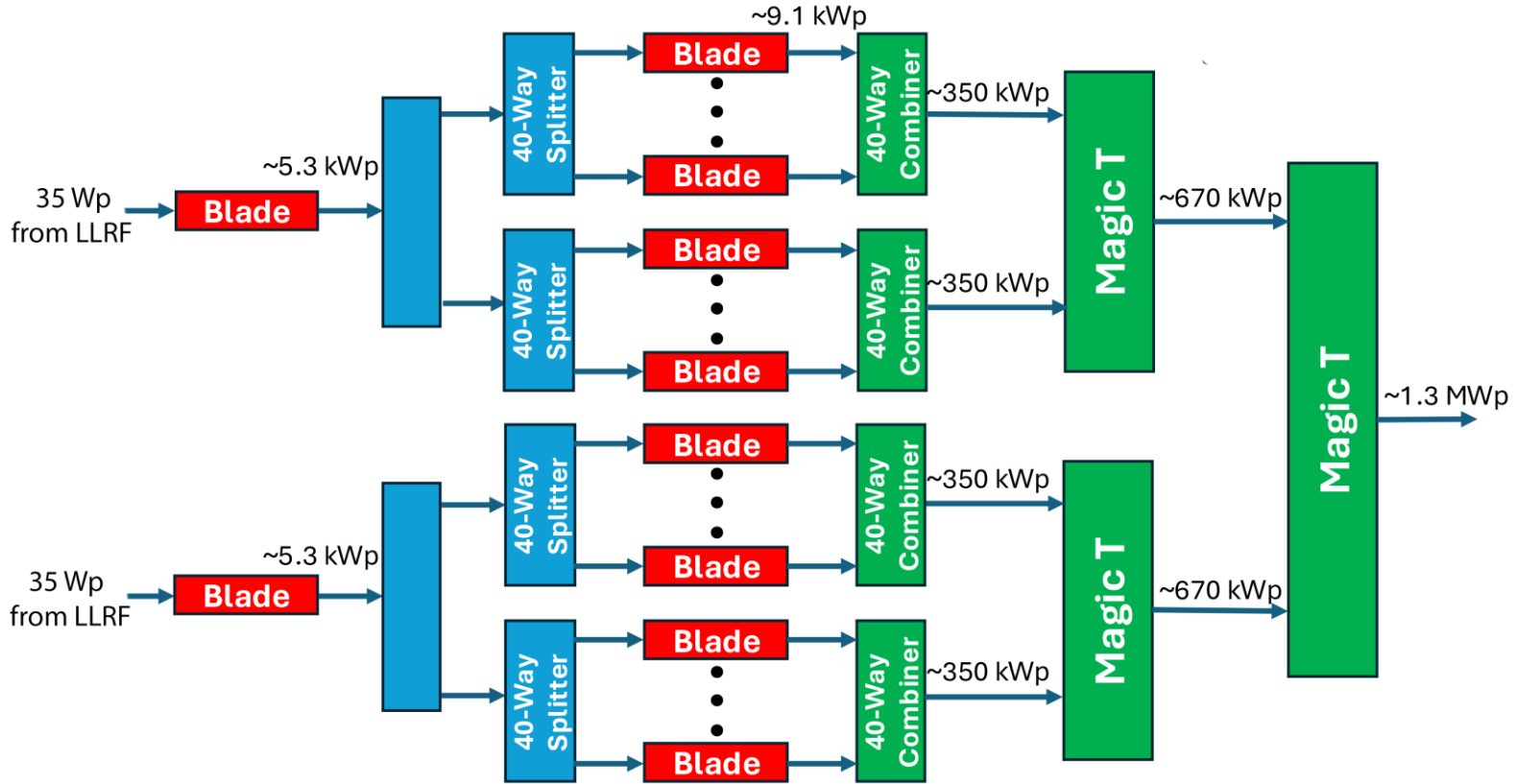
2-Way Isolated Gysel Combiner



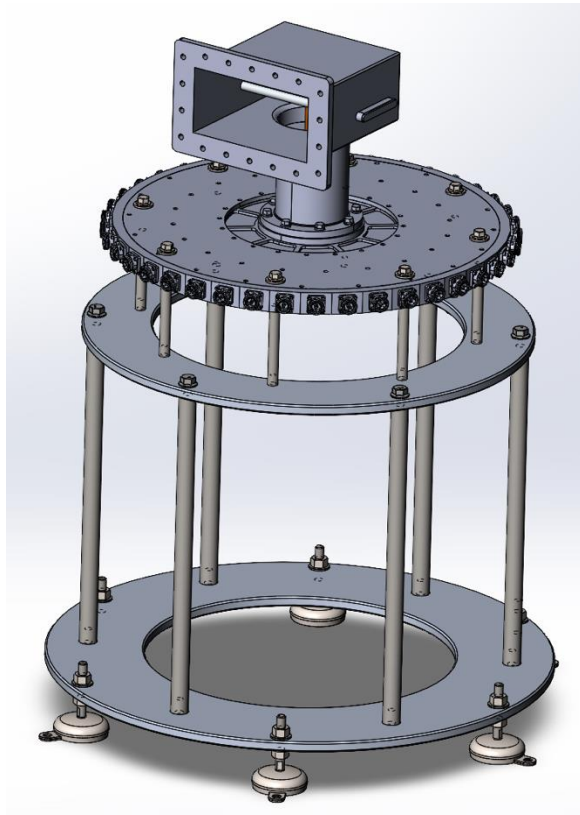
Blade Cooling Details



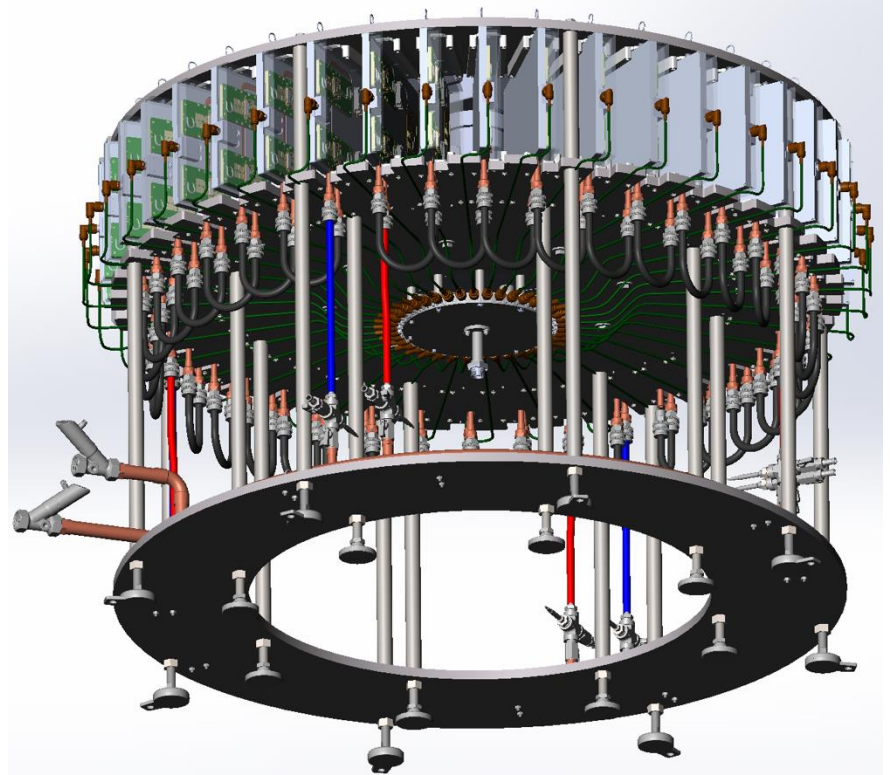
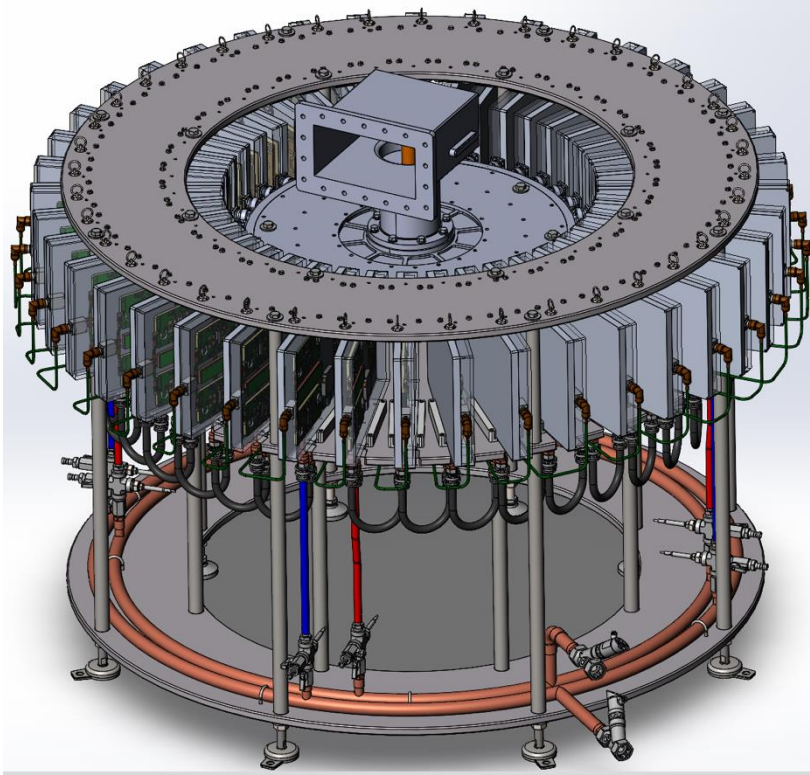
Overall Power Amplifier RF Power Flow



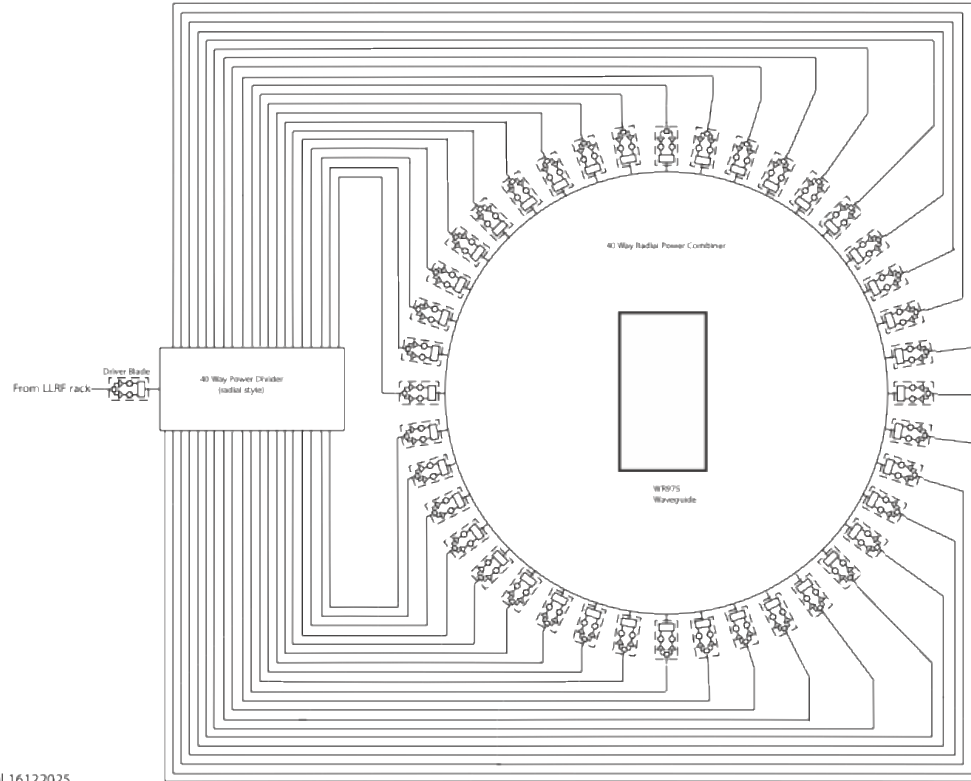
40-Way Radial Power Combiner



1/4 Power ~ 350 kWp

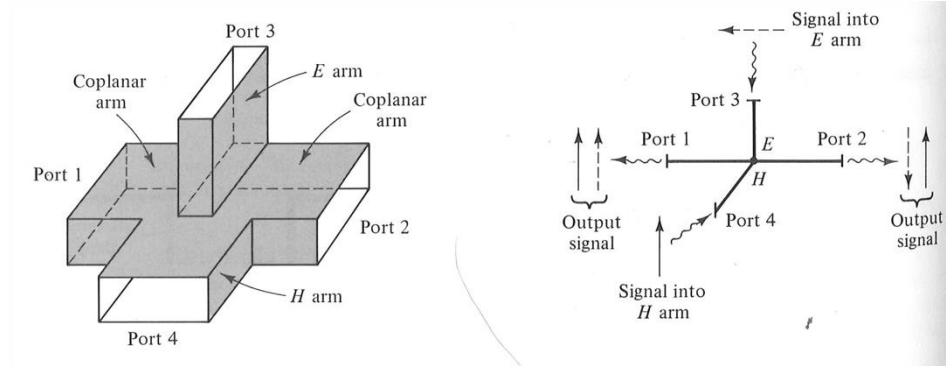


1/4 Power RF Power Flow



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Magic Tee High Power Combiners

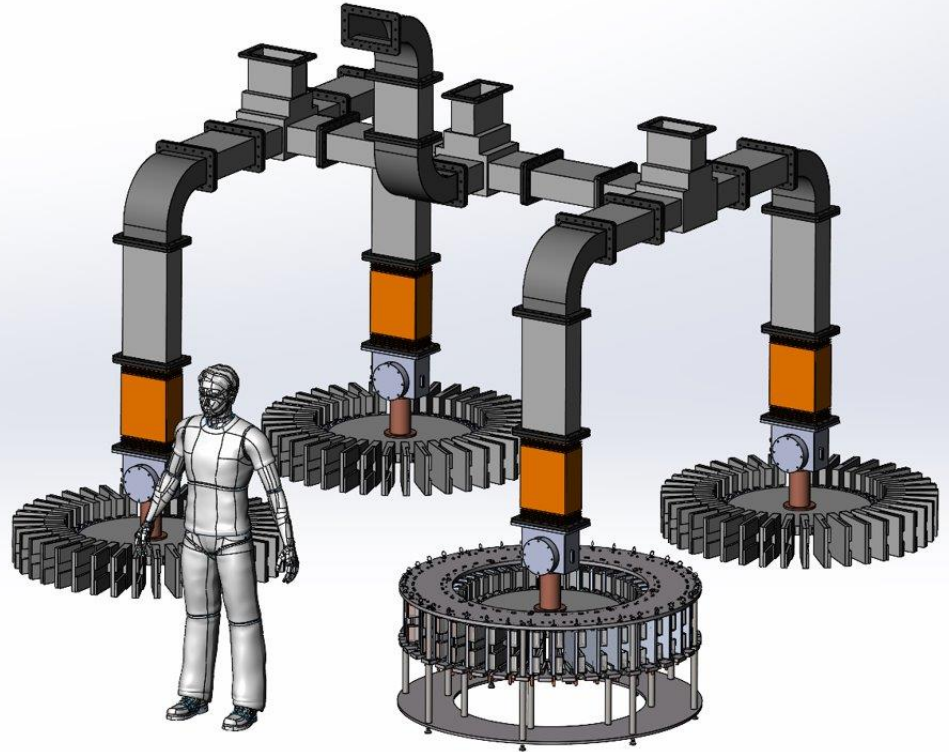


From Rizzi, *Microwave Engineering – Passive Circuits*

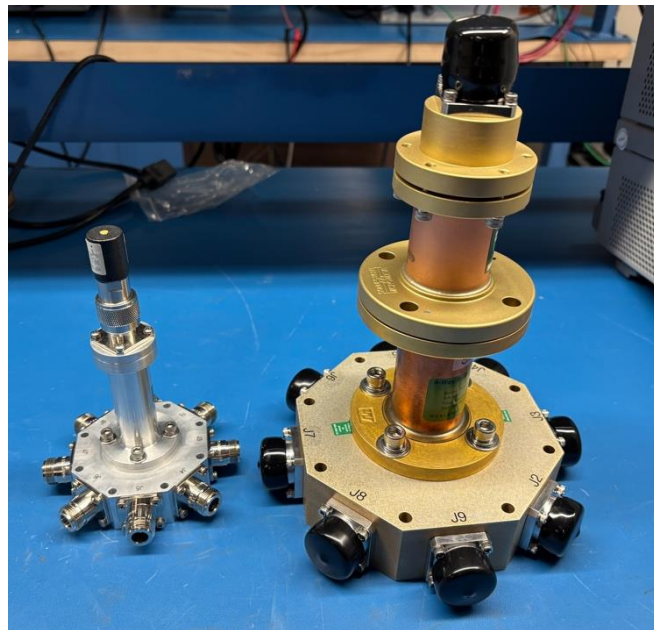
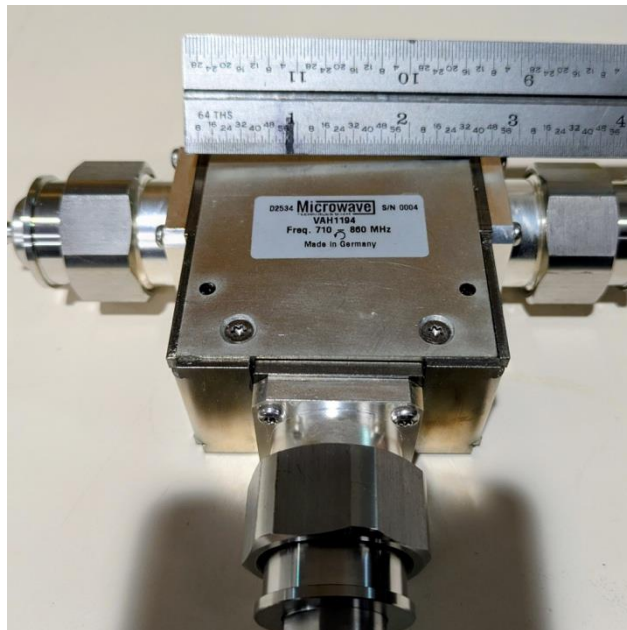


Full 1.25 MWp Amplifier

- All elevated aluminum waveguide is lightweight, including magic Tee's
- 3 Water loads not shown, will be near floor, out of way
- Full power circulator is adjacent to shielding shaft to CCL
- 100 VDC power supplied from area of original HV capacitor bank, replaced with LV capacitor bank and AC/DC converters, four per system



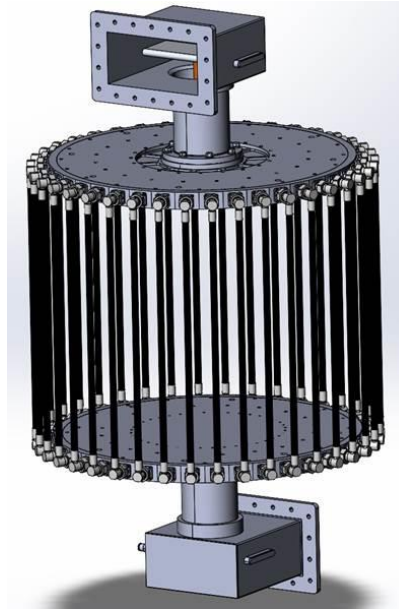
Passive RF Components in Test



- 5 kW circulators vary greatly, even with temperature
- Measuring S-parameters in temperature chamber

8 way radial divider and combiner
for 50 kW scaled test this year

Passive RF Components – High Power Test



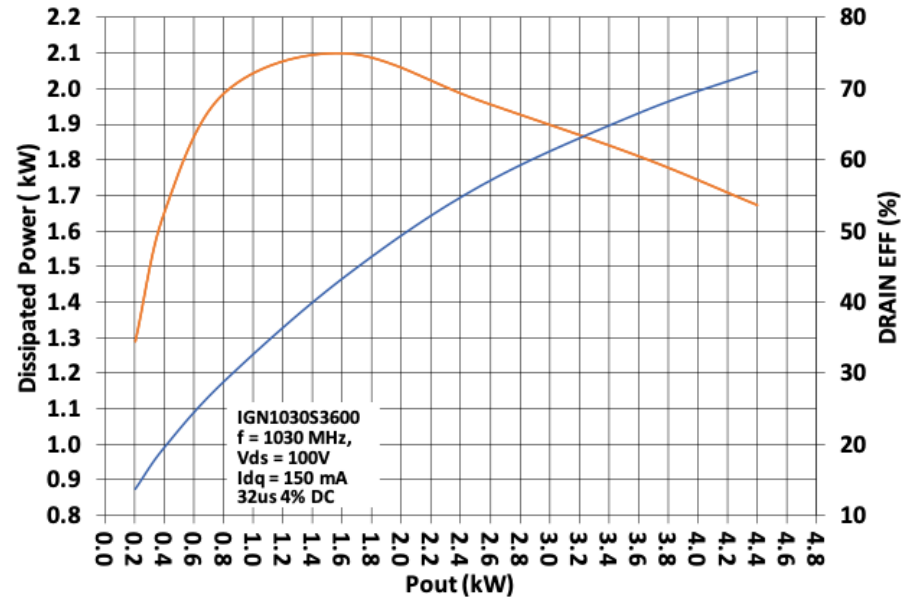
- 40-Way radial power combiner test setup, back-to-back with phase matched cables (10kWp each)
- Will drive this with a klystron and use a water load, in collaboration at SNS
- Thermal test for average power and peak power test for voltage
- Vendor will attend testing

Varying CCL power requirements at different locations

- **Turning down drive power is a concern for Class AB devices with fixed V_d**
 - When conditioning a CCL cavity
 - Ramping up power slowly
 - During accelerator beam tuning
 - Normal uneven RF power distribution along linac from physics tune
 - Fast power fluctuation for beam loading
- **Need about 14 dB of output dynamic range for these situations, 50 – 1250 kW**

GaN Thermal Measurement at Integra Technologies

- Thermal measurement performed at worst case conditions
 - This is for another transistor, not IGN815
 - Worst case power dissipation of 1.87kW
 - Flange temperature = 85°C
 - Transient infrared detector used to capture peak temperature during RF pulse

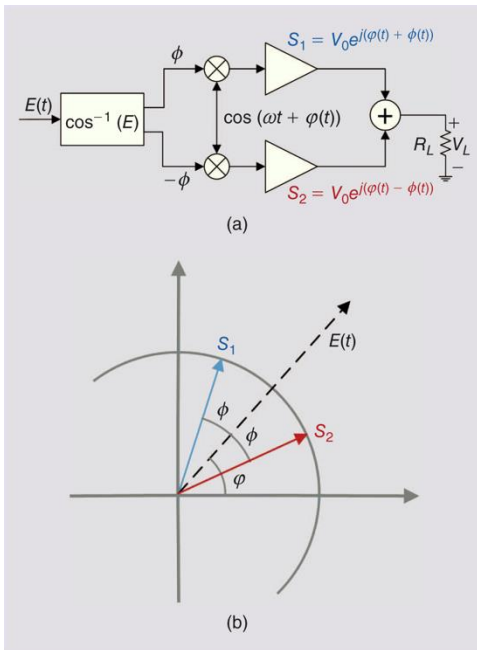


This property of Class AB amplifiers can kill transistors during power rollback

Techniques for Variable Power to Avoid High P_d

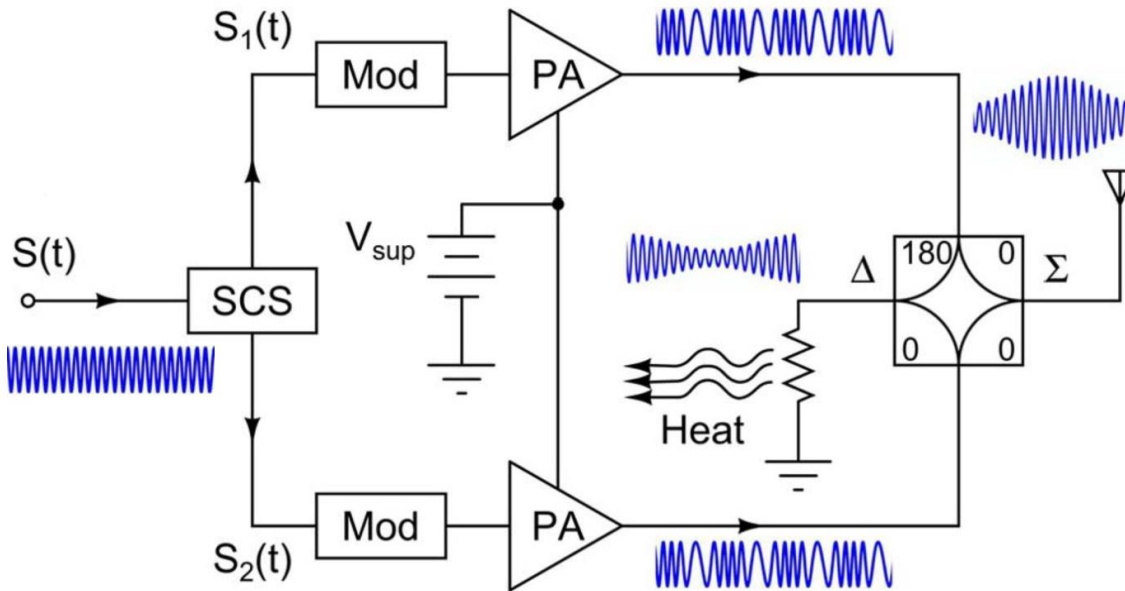
- **Reduction of V_{ds} below 100 V to keep high efficiency at lower power**
 - 20% is safe but it cannot be fast with large power converters
 - How would it be automatic?
 - Below 70 V could cause K factor instability
- **Turning off pallets before combiner**
 - Must account for reverse power to other pallets
 - Modeling is being done to understand which ones are best
 - Difficult to remove RF driver power from a common driver amp, but could raise gate bias via logic signal to disable output
- **Outphasing modulation for fast control, beam compensation**

Outphasing Modulation, with Two PAs driven into Saturation



**Vector representation
of outphasing transmitter**

(from Barton, IEEE Microwave Magazine, Feb. 2016)



**Components before PA are generated in I/Q digital LLRF,
creating two phase modulated signals of constant amplitude**

(Adopted from Godoy, IEEE Trans MTT, Dec. 2009)

